

A 0.3V Biofuel-Cell-Powered Glucose/Lactate Biosensing System Employing a 180nW 64dB SNR Passive $\Delta\Sigma$ ADC and a 920MHz Wireless Transmitter

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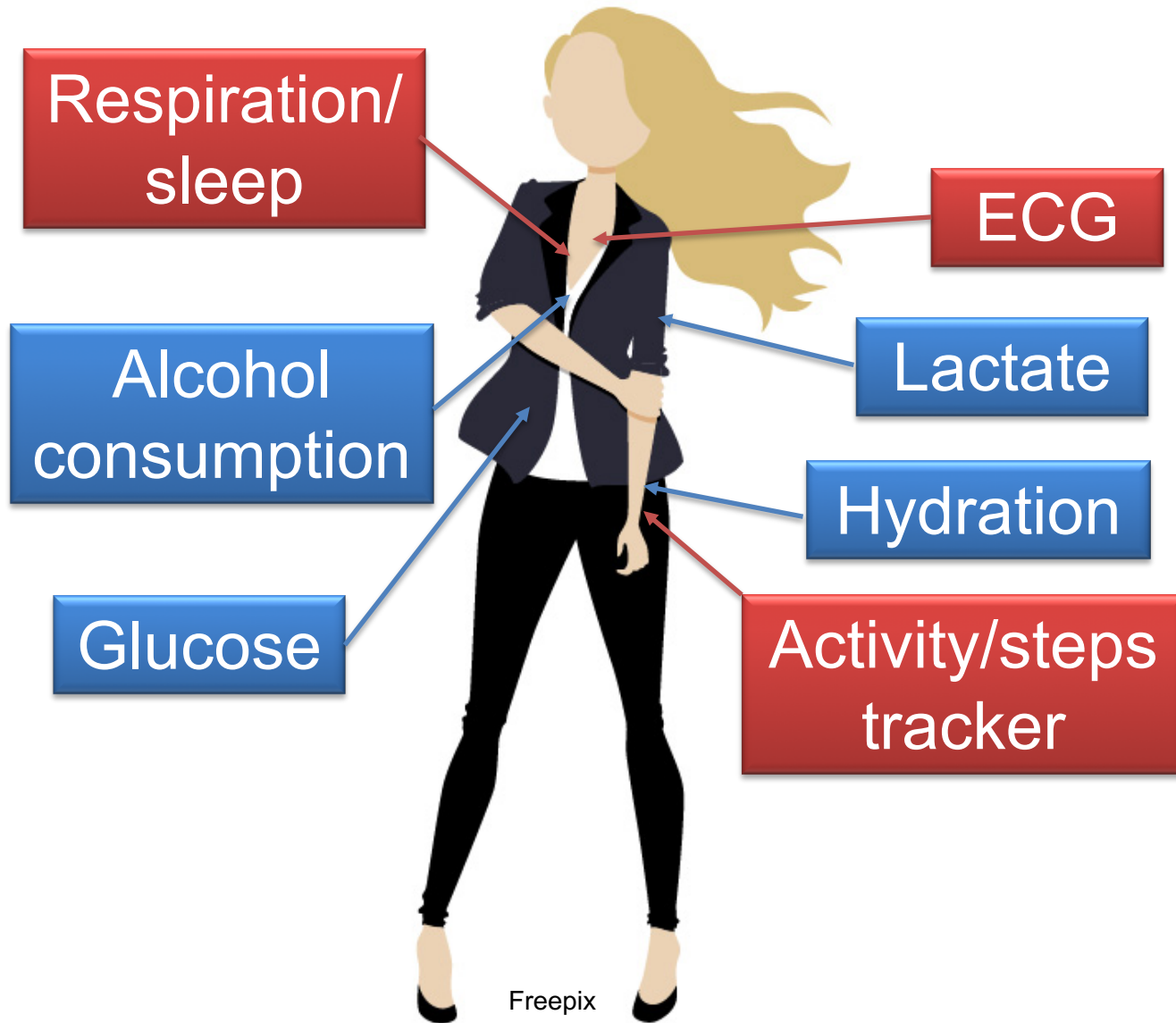
¹Department of Electrical and Computer Engineering

²Department of NanoEngineering

³Now with GenapSys Inc.



Next-Generation Wearable Sensors



SENSING TODAY:

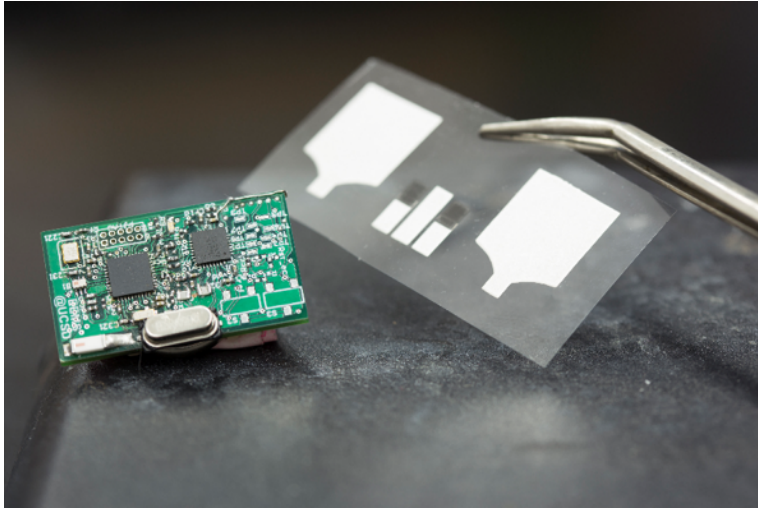
- Physical parameters
 - Electrophysiology
- *Limited utility in daily life*

NEXT-GENERATION:

- Physiochemistry
- *More actionable information for daily life improvement*

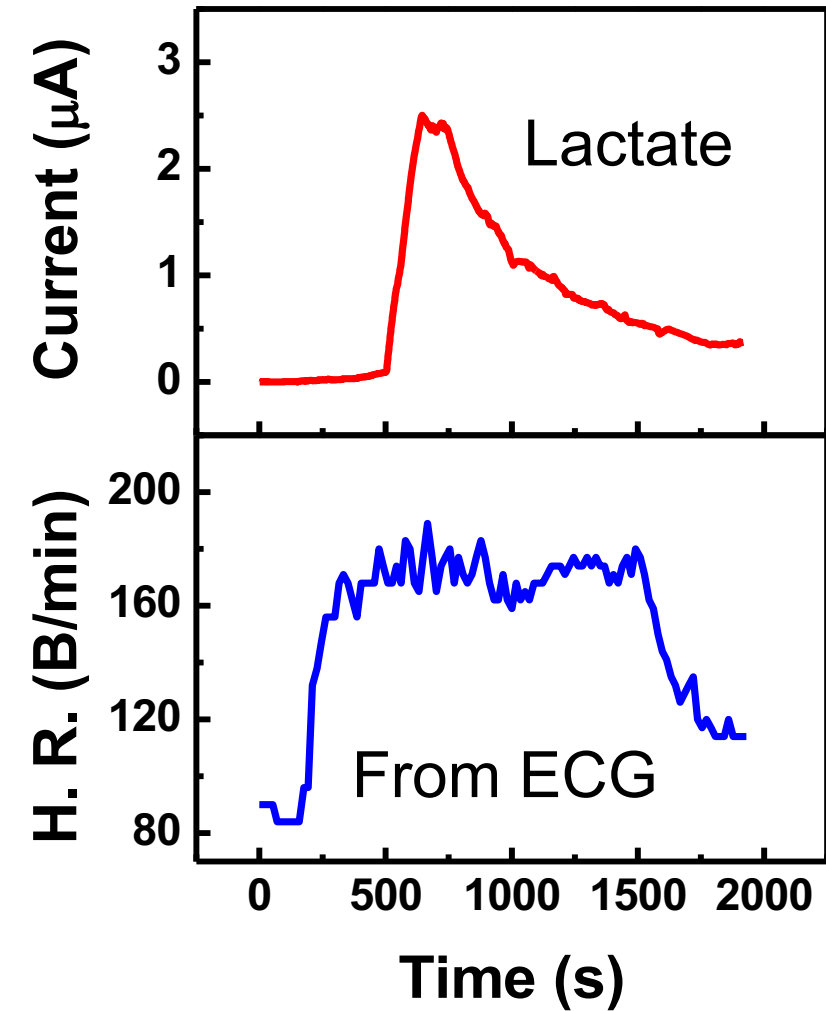
Research need: wireless physiochemical sensors

Wireless Physiochemical Sensing



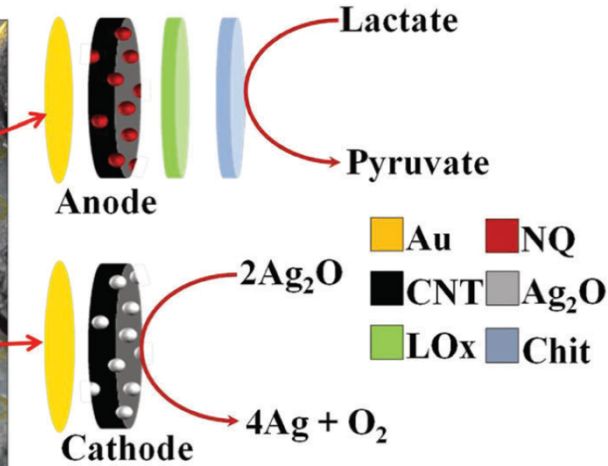
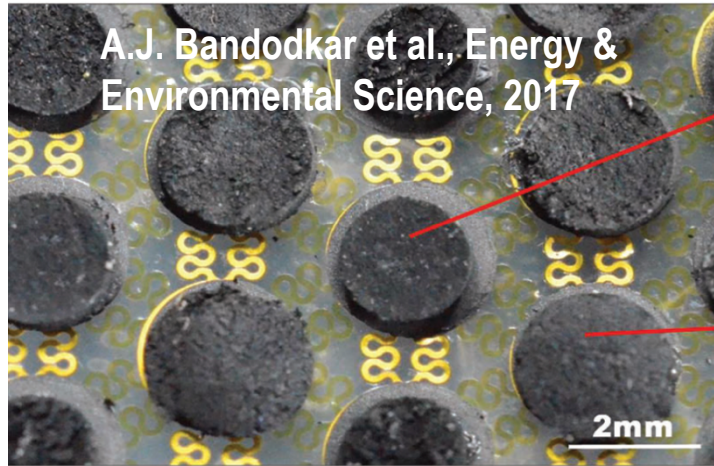
First demonstration of simultaneous real-time electrophysiology + physiochemical sensing
Requires battery, power management, user interaction

Research need: wireless physiochemical sensors that are small, unobtrusive and self-powered: “*unawearables*”



S. Imani et al., Nature Communications, May 2016

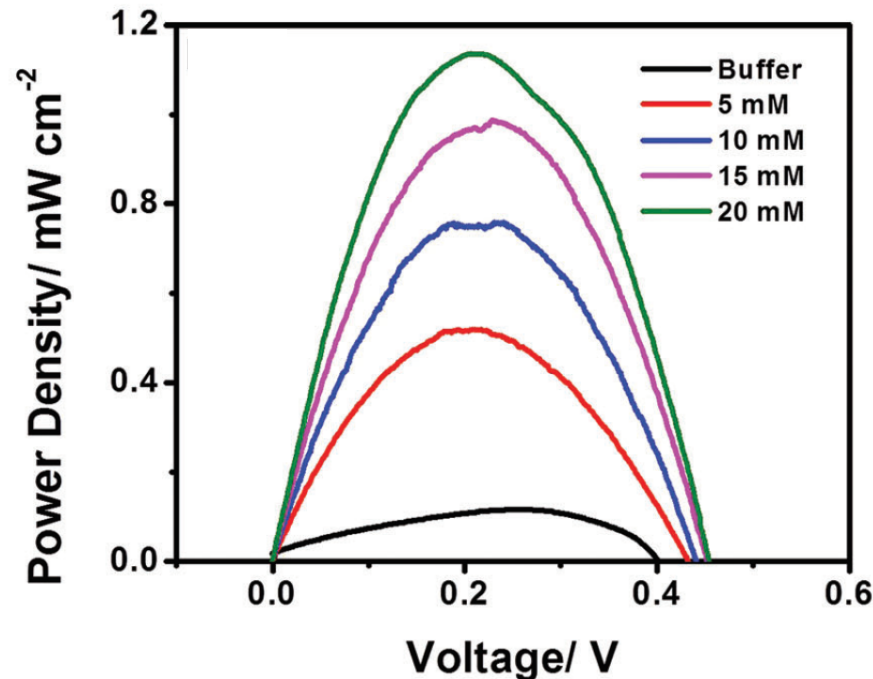
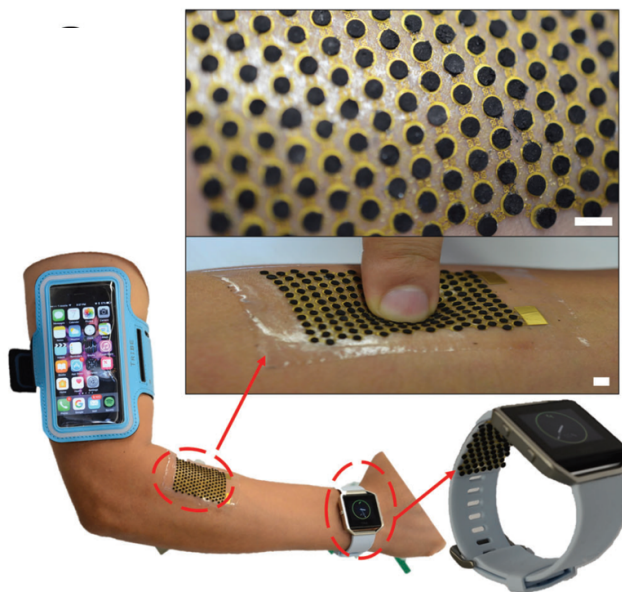
Physiochemical sensing and energy harvesting



- Biofuel cells (BFCs) convert biofuels (e.g., glucose, lactate) into electrical power
- Power \propto fuel concentration

IDEA: utilize BFC power to create a self-powered physiochemical sensor

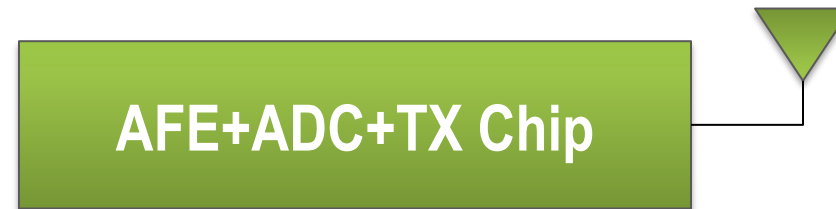
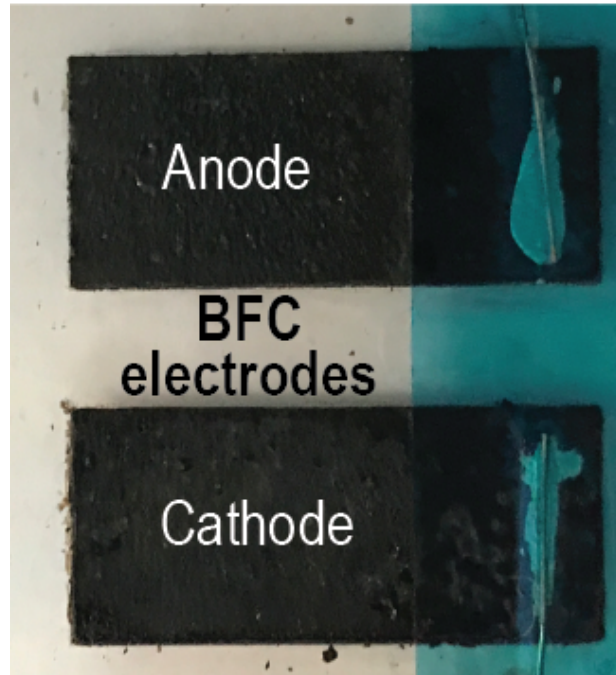
CHALLENGE: do so reliably, and in a small form factor (no DC-DC converter)



Outline of the Presentation

- 1. Biofuel Cell Material Composition**
- 2. Proposed Biosensing System Architecture**
- 3. System Implementation**
 - **AFE**
 - **$\Delta\Sigma$ ADC**
 - **Wireless Transmitter**
- 4. In-Vitro Experimental Results**
- 5. Conclusions**

BFC Material Composition



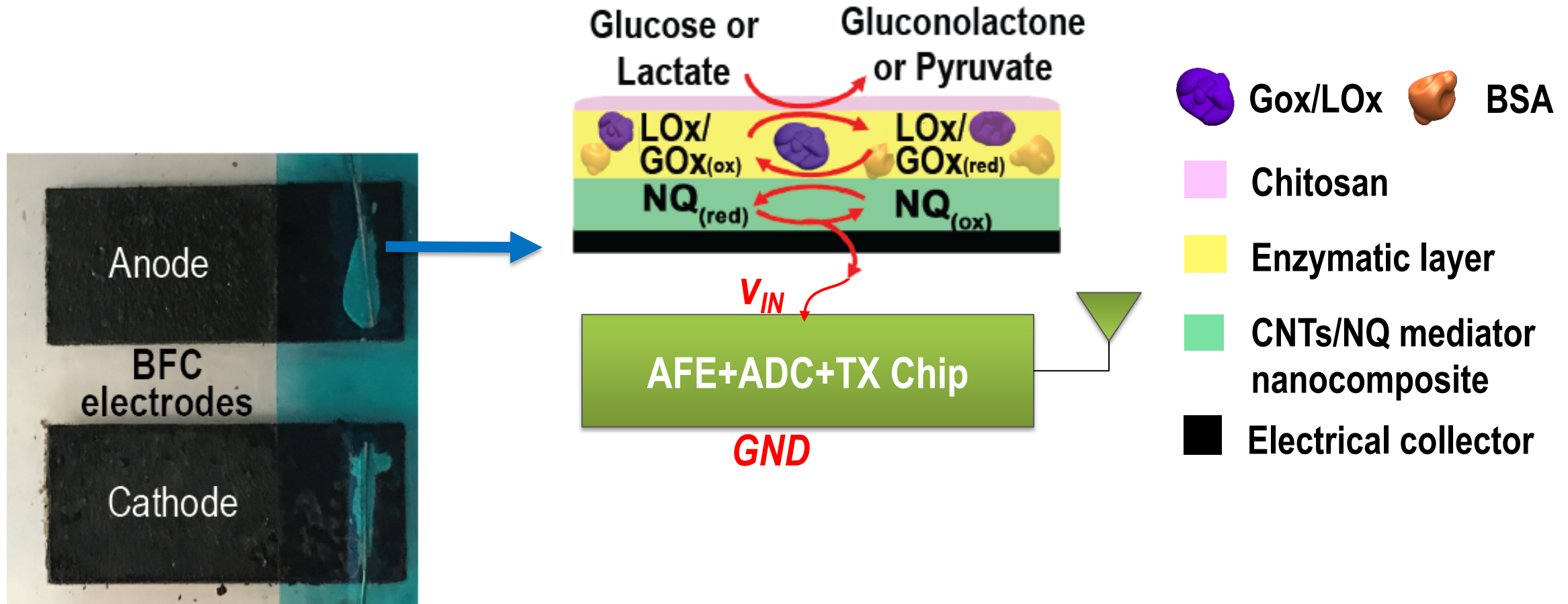
- Custom-fabricated lactate and glucose biofuel cells (BFCs)

BFC Material Composition



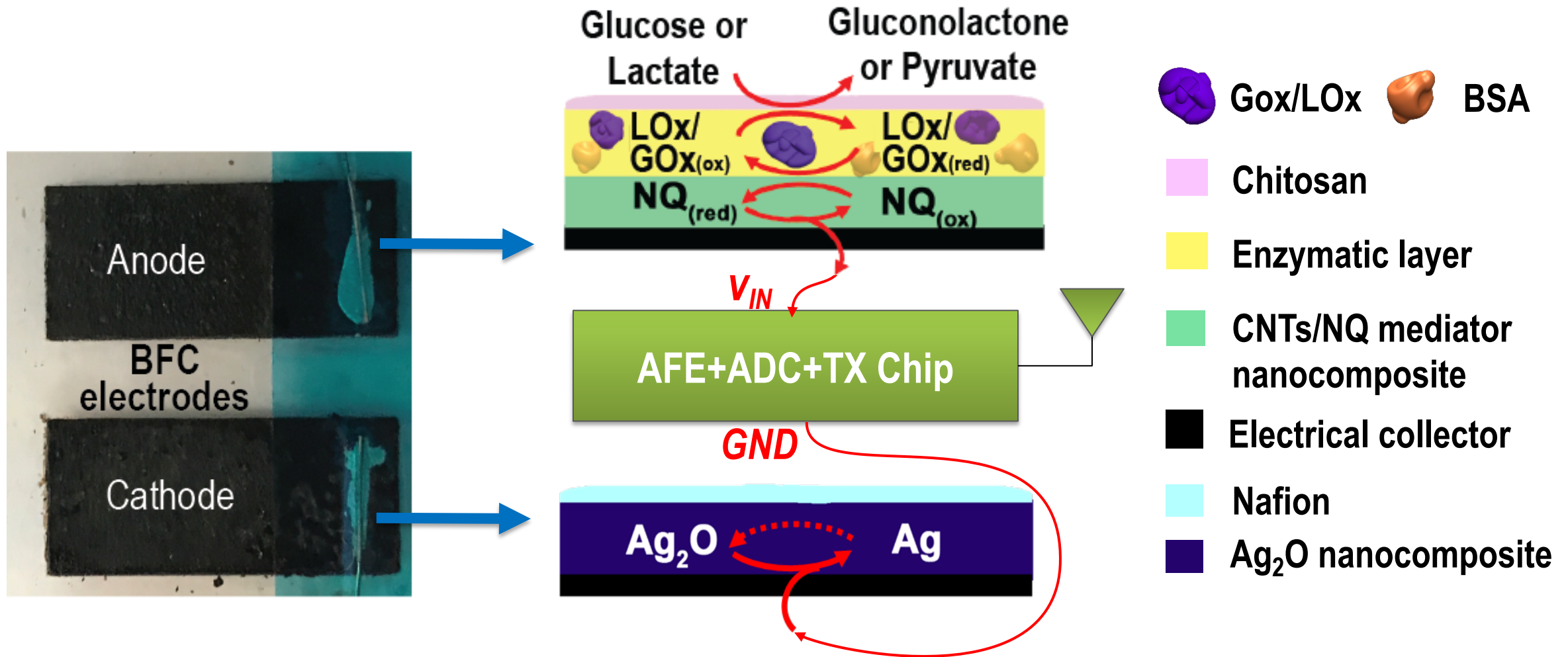
- BFC anodes material composition

BFC Material Composition



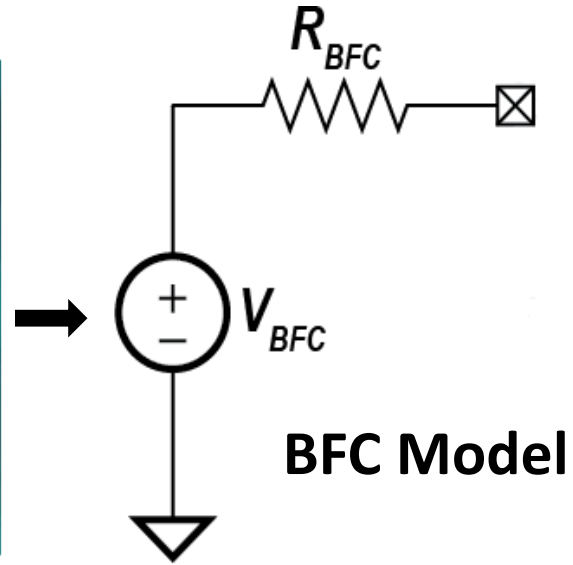
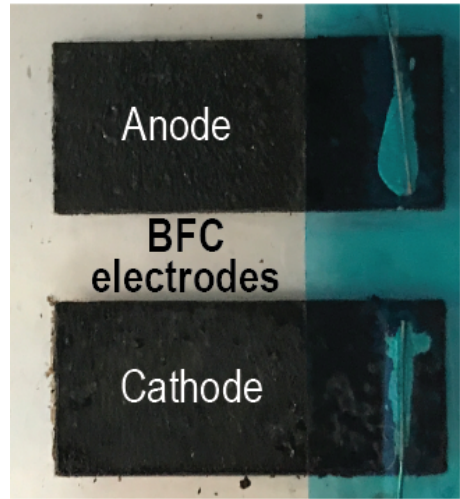
- Enzymatic cocktail consisting of lactate or glucose oxidase

BFC Material Composition



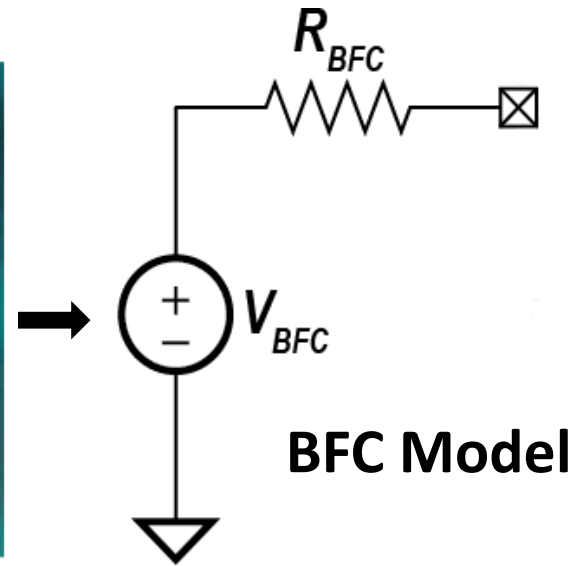
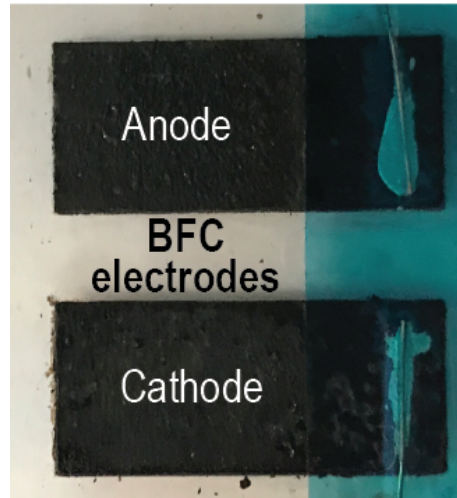
- BFC cathode material composition

Biosensing System Architecture



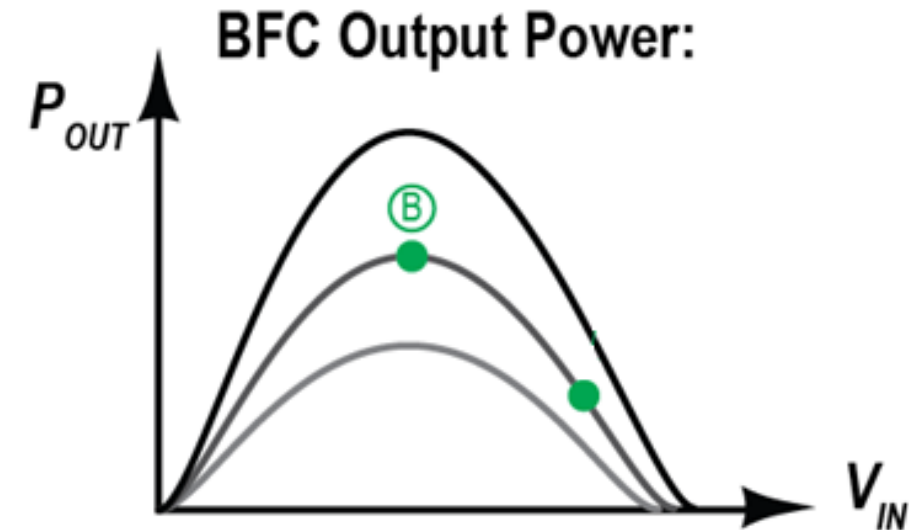
- Steady-state BFC model

Biosensing System Architecture

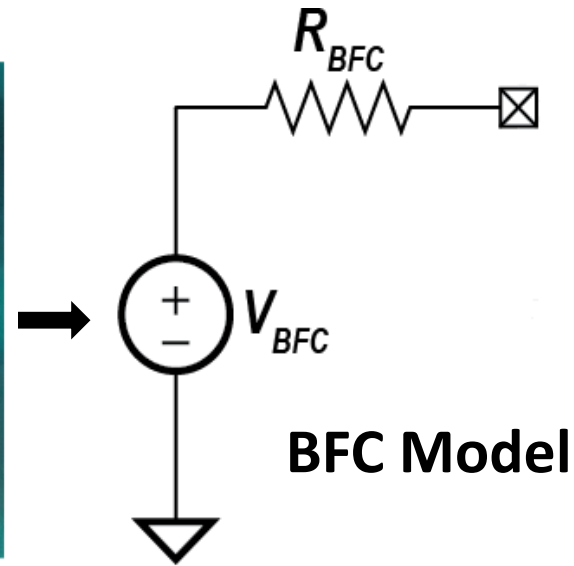
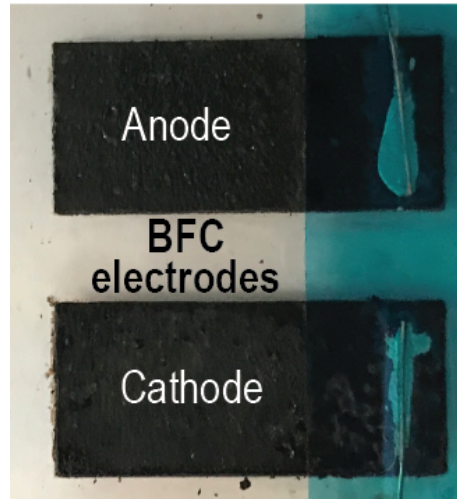


- Linear correlation of maximum power point (MPP) of the BFC (point B) with fuel concentration

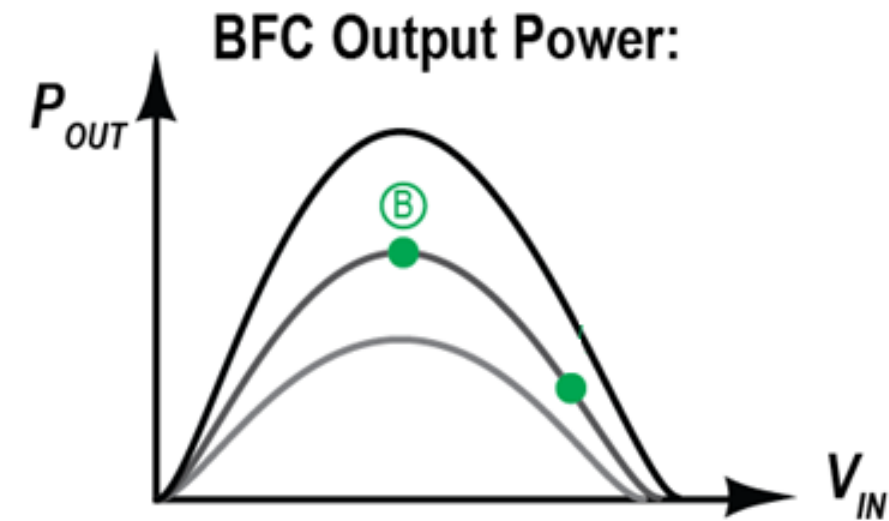
How to measure MPP?



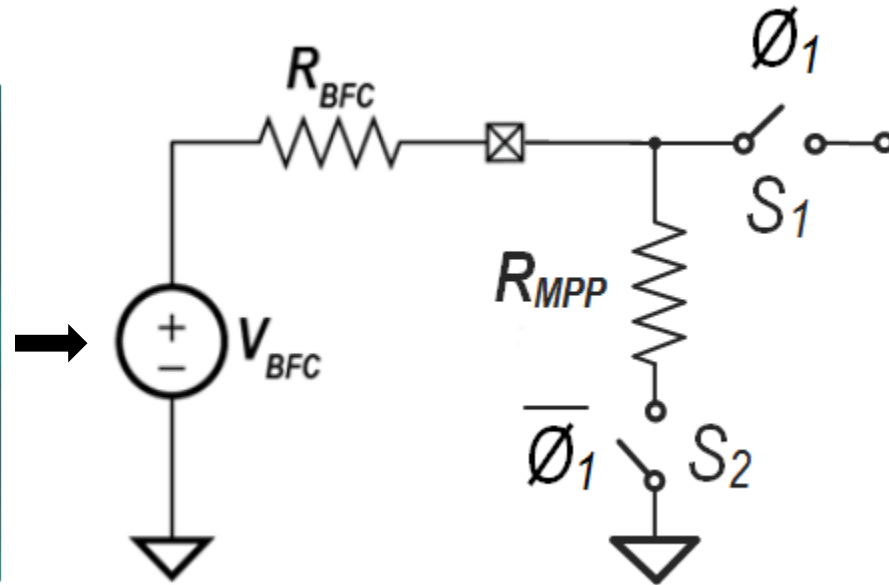
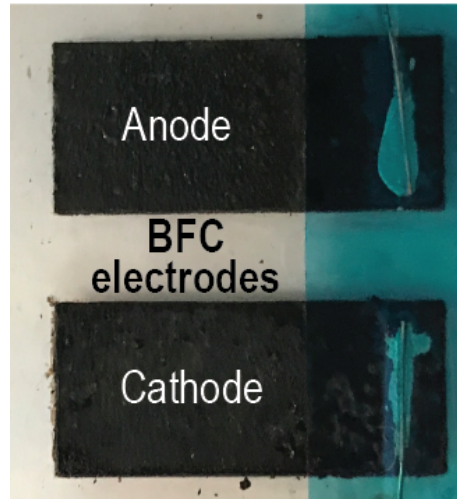
Biosensing System Architecture



- **To measure maximum power point (MPP)**
 - DC-DC converter for MPP tracking
 - Bulky inductors, large power



Biosensing System Architecture



- **To measure maximum power point (MPP)**

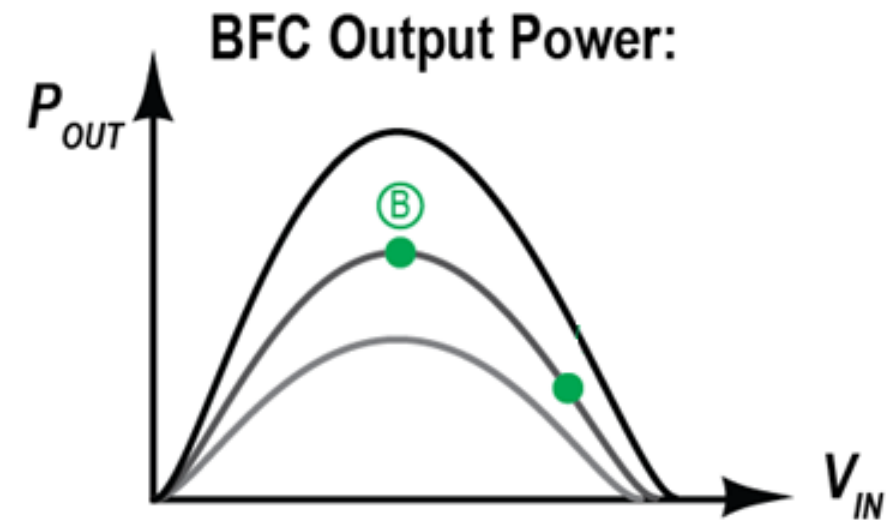
- DC-DC converter for MPP tracking

→ Bulky inductors, large power

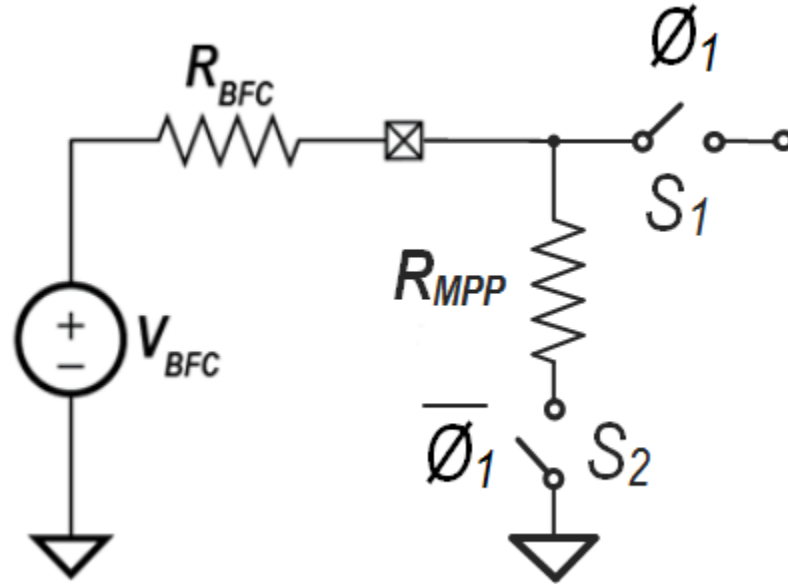
- Always presenting a matched load

→ Limits longevity

- Periodically presenting a matched load (here with a 1% duty ratio)

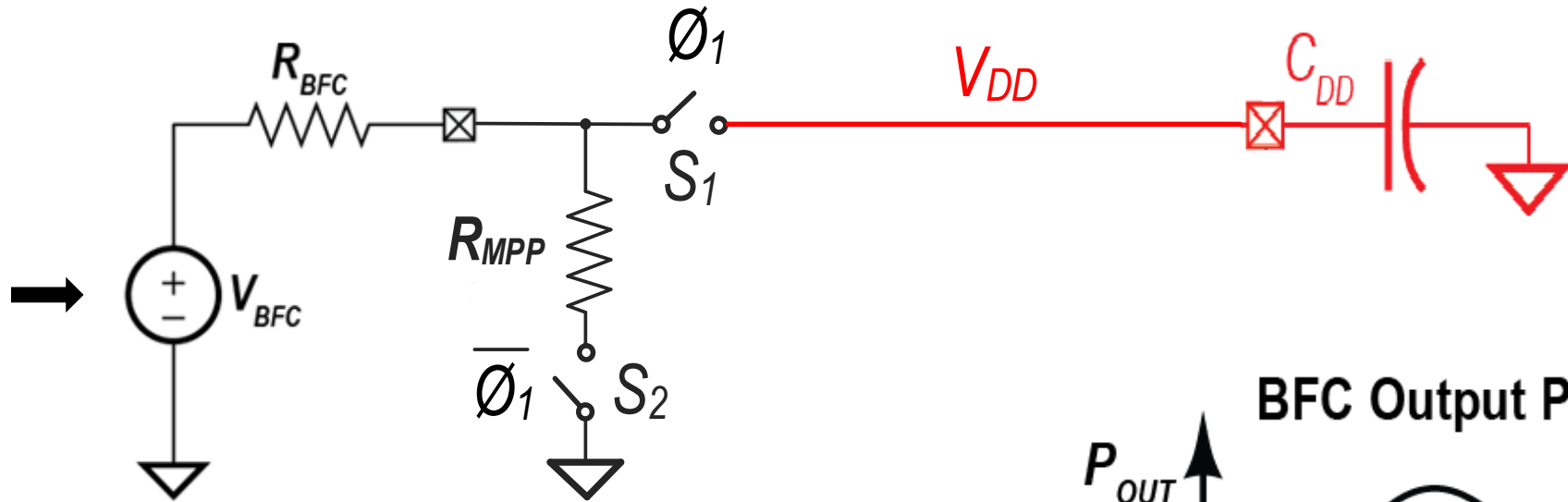
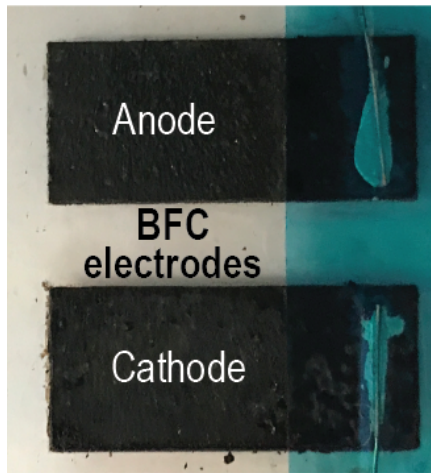


Biosensing System Architecture



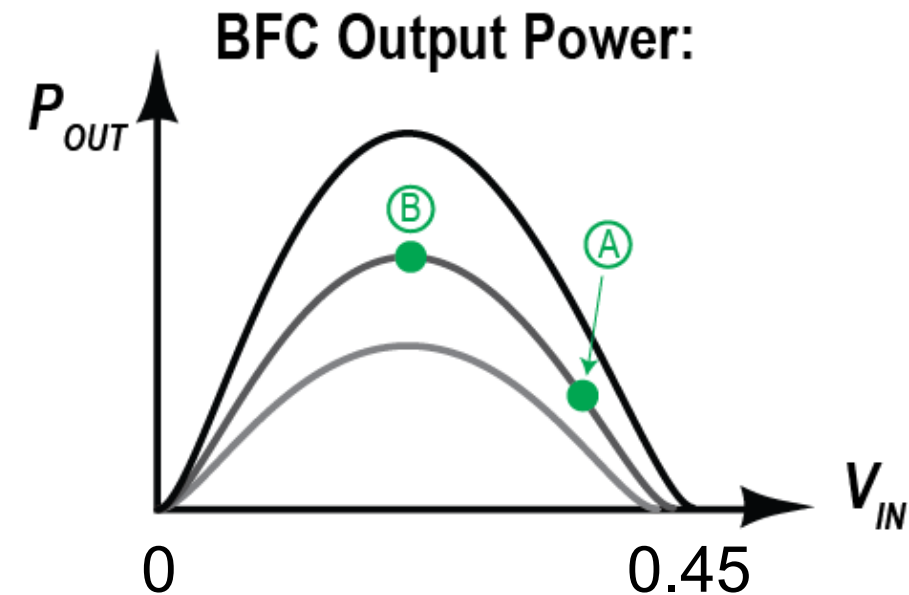
- Matched load R_{MPP} at only 1% duty ratio in this work
→ *To avoid fuel depletion at the maximum possible rate*

Biosensing System Architecture

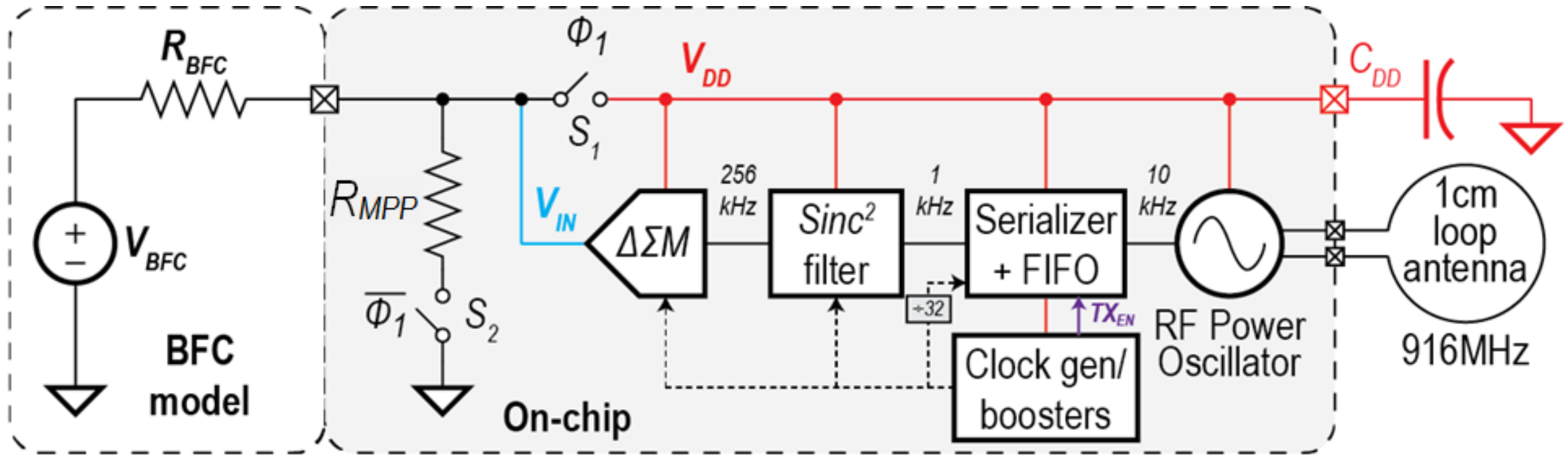


- **To minimize the rate of fuel consumption**
 - Average power is kept much less than the BFC's MPP (point B)
 - V_{DD} near the open-circuit (point A)
- **The BFC open-circuit is relatively large**

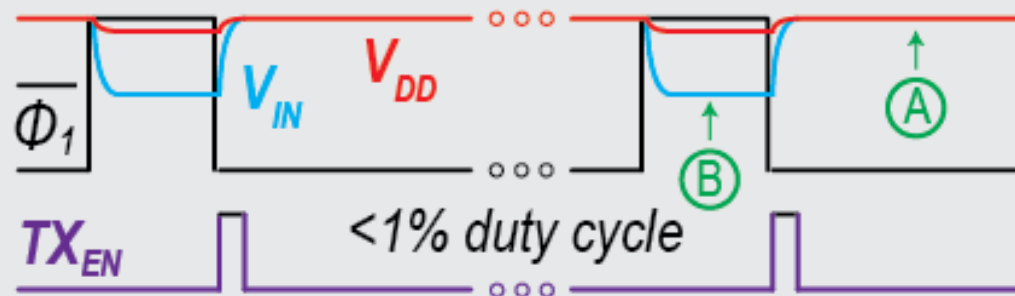
→ We need no DC-DC converter



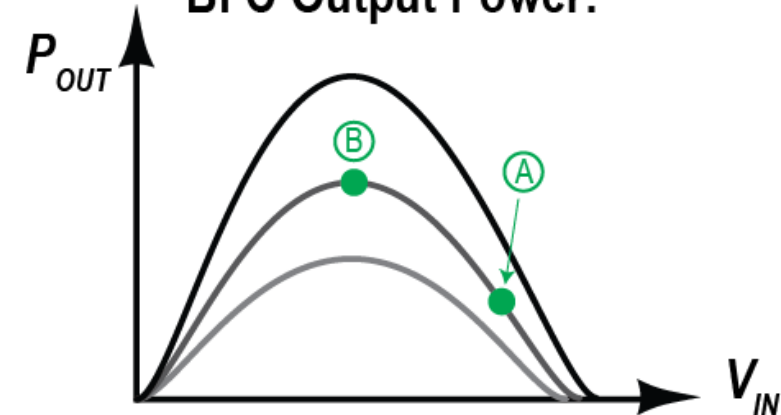
Biosensing System Architecture



Timing diagram:



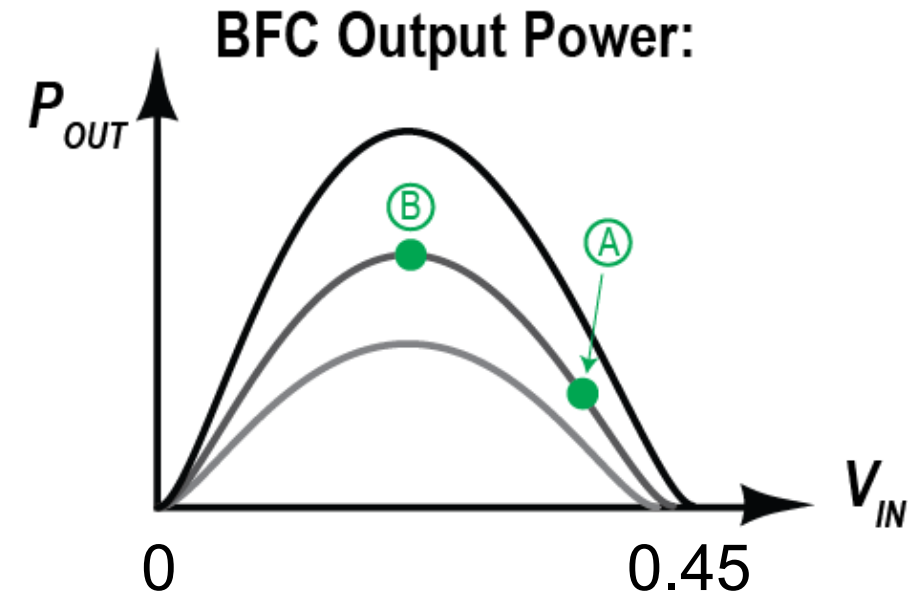
BFC Output Power:



Circuit Design Requirements

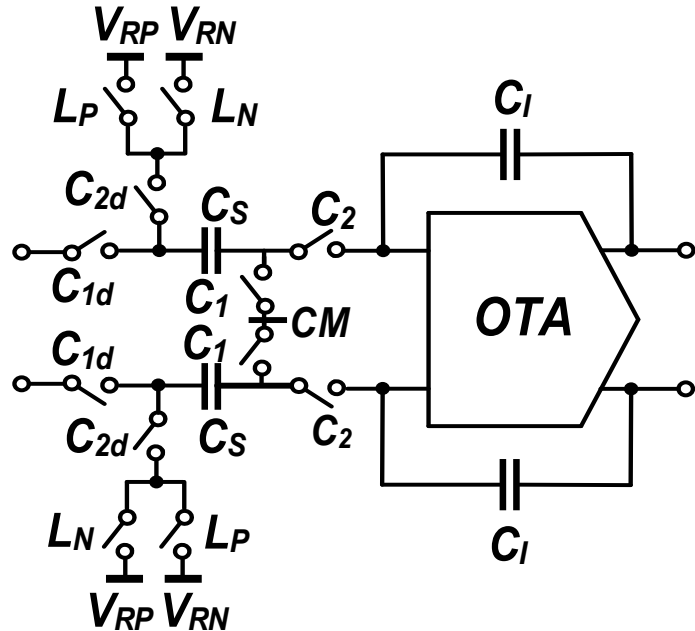
Circuit Design Limitations:

- BFC's open circuit voltage $< 0.45V$
 - *Complete integrated wireless biosensor must operate at 0.3-0.4V*
- Limited underlying fuel energy
 - *Low energy consumption*



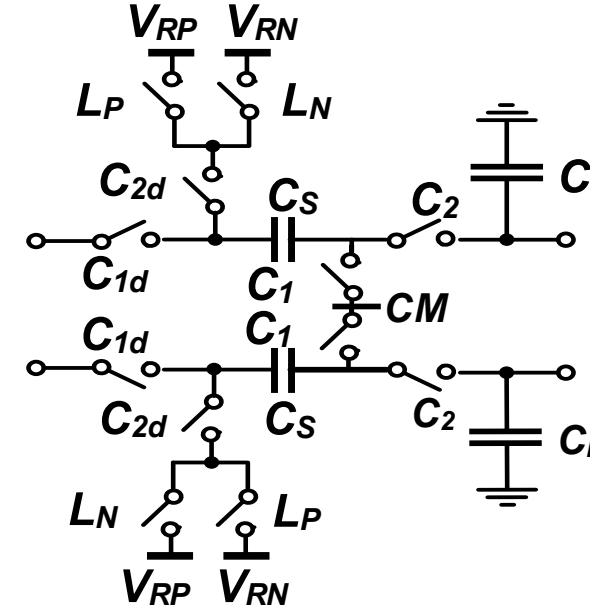
$\Delta\Sigma$ Modulator Architecture

SC active Integrator



- × $1/f$ noise
- × Difficult to scale down V_{DD} to 0.3V
- × High power to attain large gain/low noise
- × OTA output swing $V_{DD} - 2V_{DSAT} \sim 0.1V$
- ✓ Lower area, $C_I = 5pF$

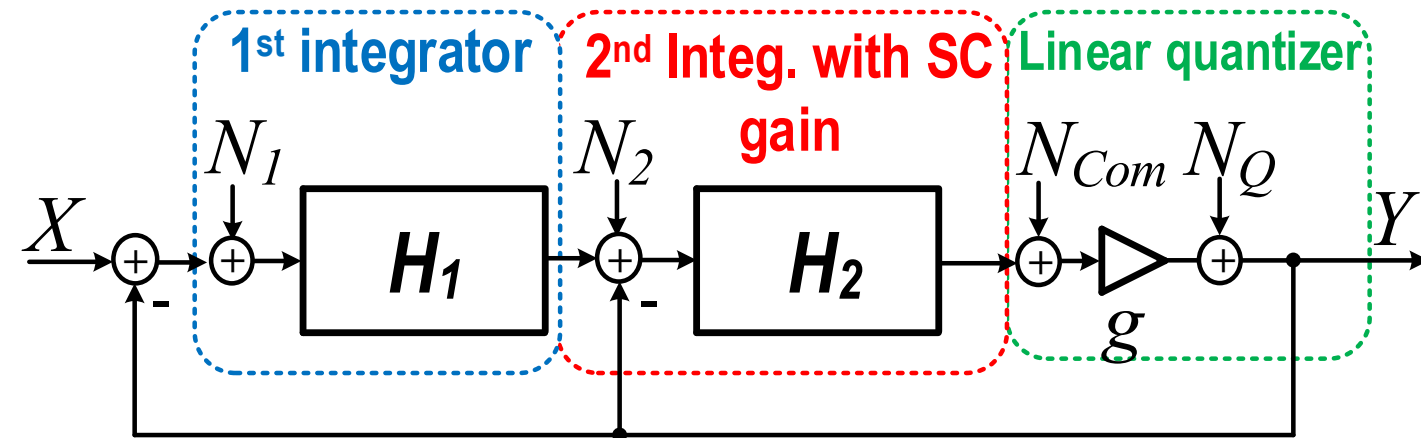
SC Passive Integrator



- ✓ $1/f$ noise free
- ✓ Easy to scale down V_{DD}
- ✓ Energy-efficient
- × Leaky integrator with no gain
- × Larger area, $C_I = 30pF$

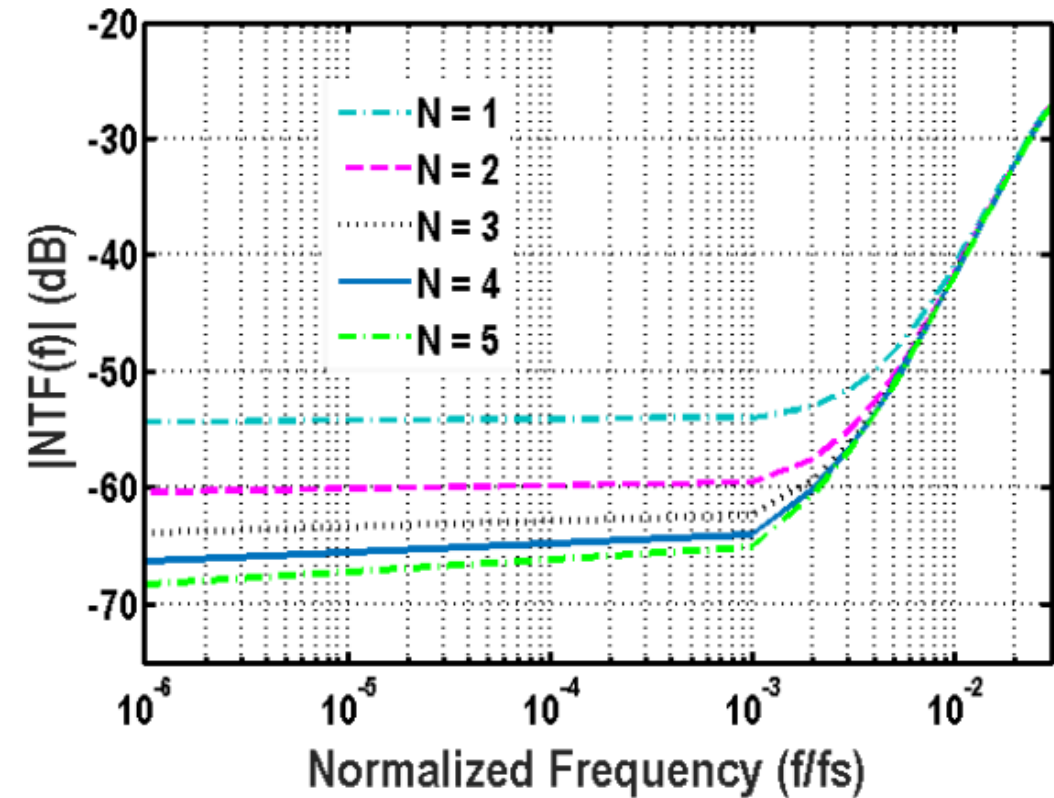
$\Delta\Sigma$ Modulator Architecture

- 2nd-order single-loop feedback architecture with 1-bit quantizer
- Energy-efficient passive filters as alternative to power-hungry active ones



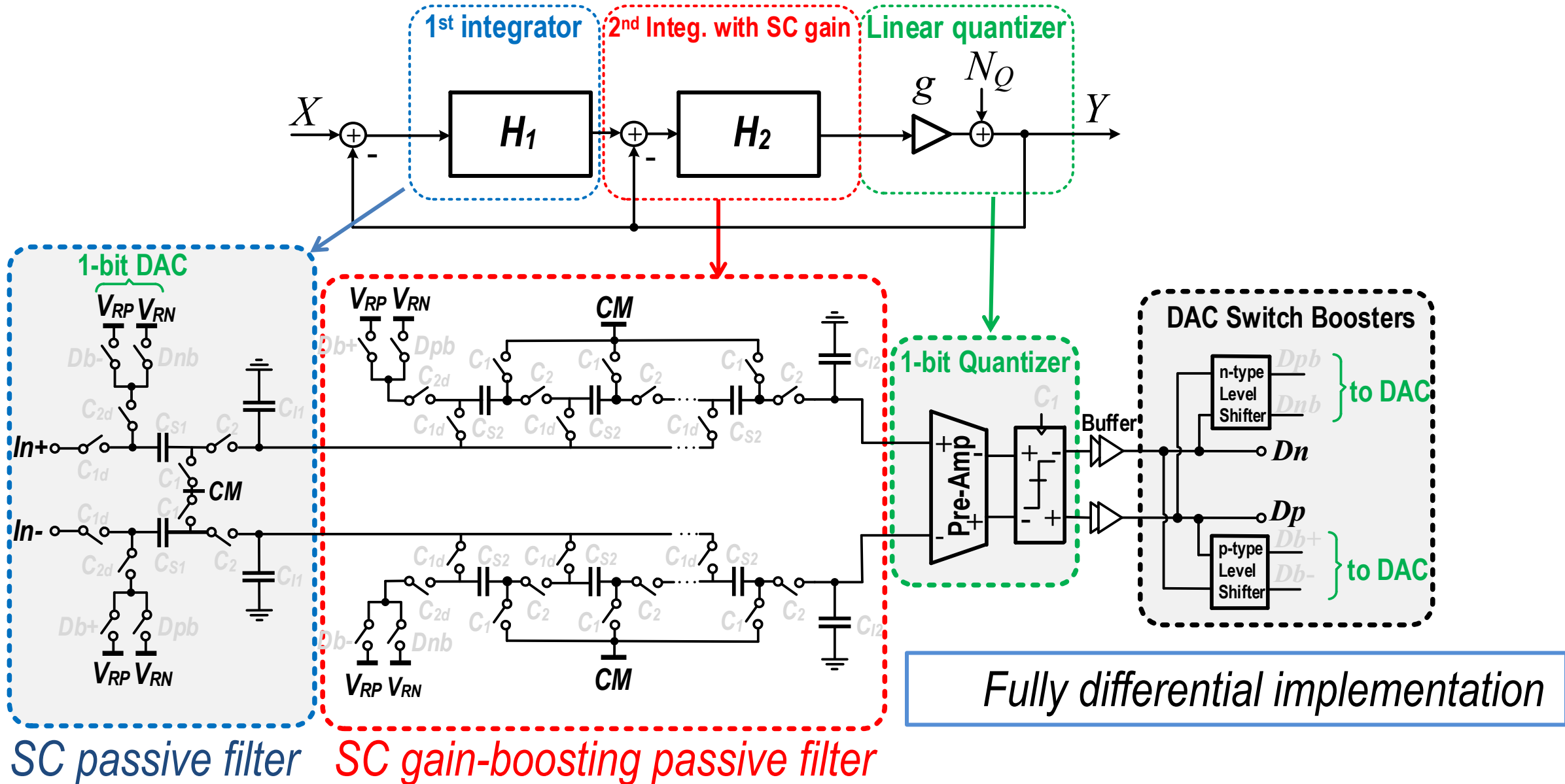
$$Y \approx X + N_1 + \frac{N_2}{H_1} + \frac{N_{Com}}{H_1 H_2} + \frac{N_Q}{g H_1 H_2}$$

$$NTF = \frac{Y}{N_Q} = \frac{1}{g H_1 H_2}$$

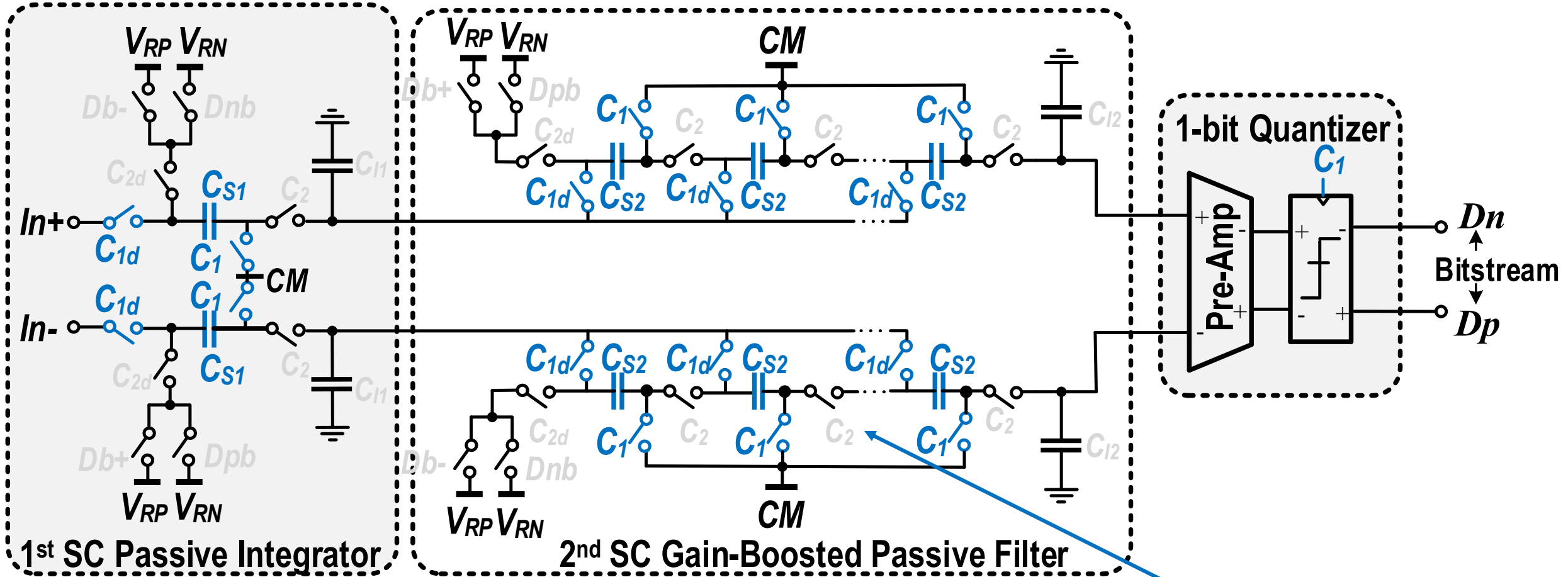


Impact of passive gain N on $|NTF|$

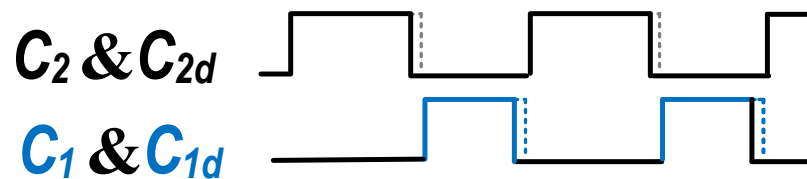
$\Delta\Sigma$ Circuit



$\Delta\Sigma$ Circuit

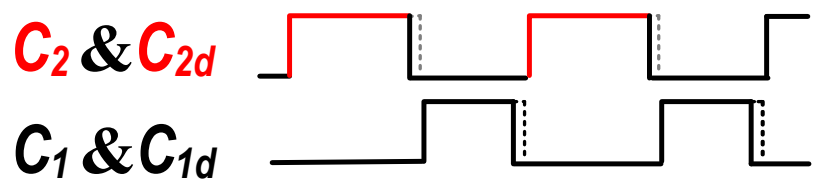
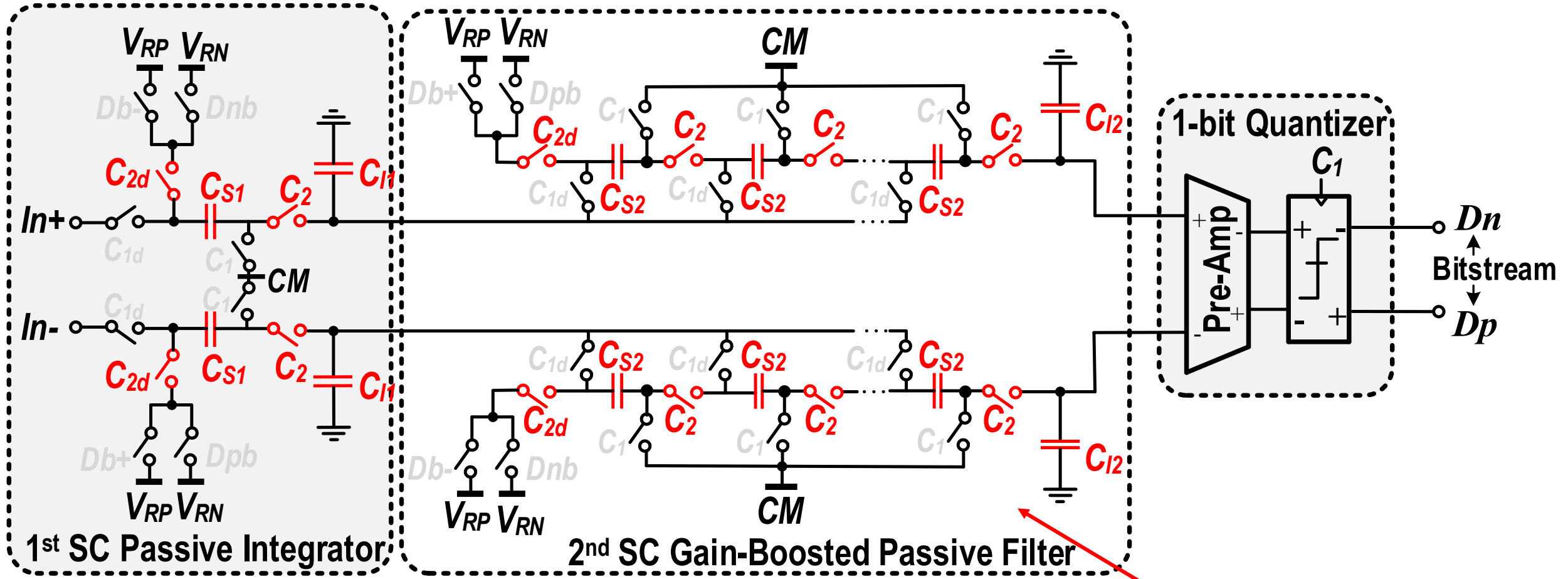


- **Charge redistribution gain-boosting scheme**



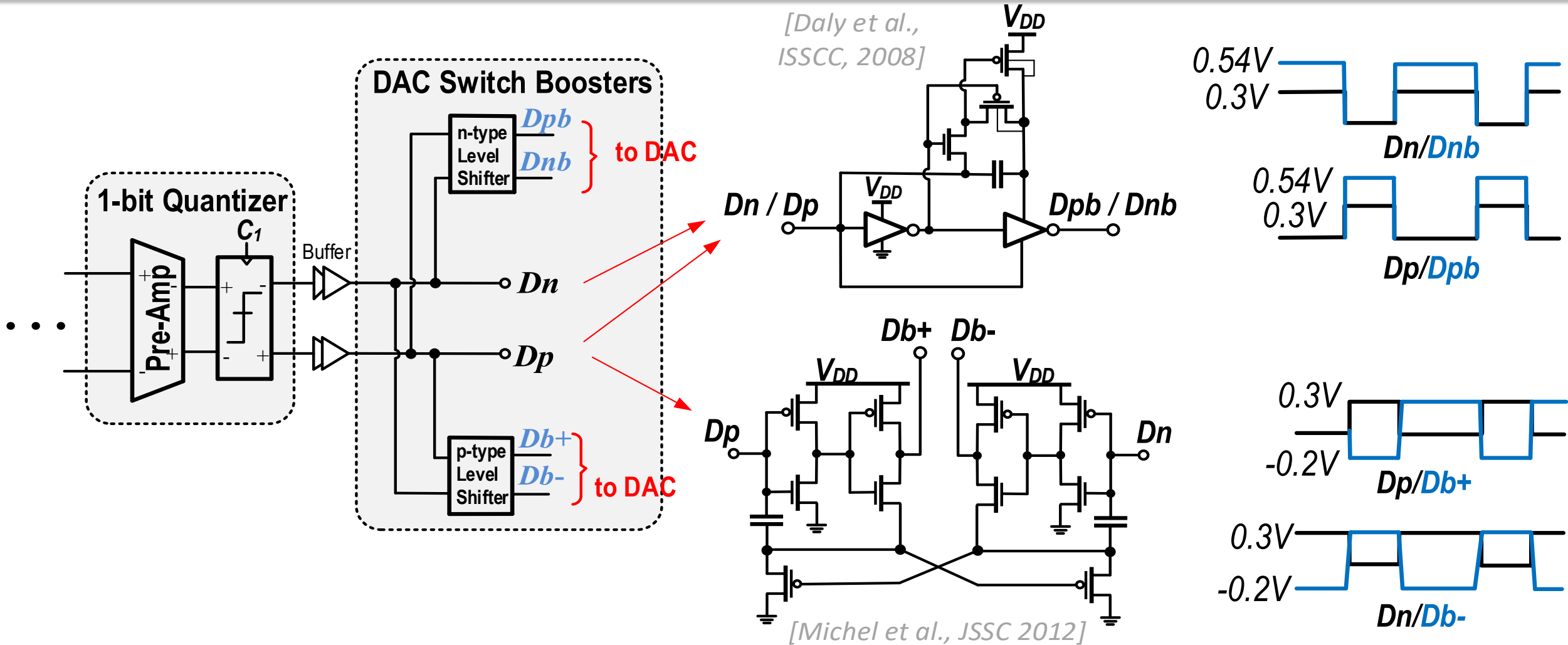
Parallel sampling onto C_{S2} s in sampling phase C_1

$\Delta\Sigma$ Circuit



Precharged C_{S2} s are positioned in series to charge share with C_{I2} in integrating phase C_2

0.3V $\Delta\Sigma$ Circuit Design



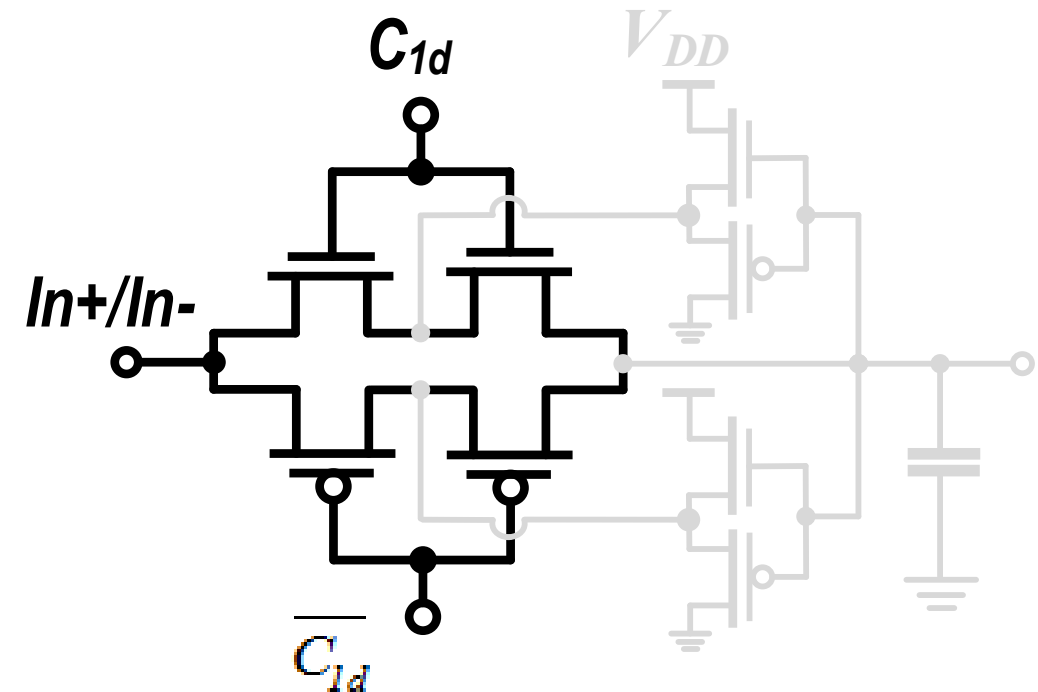
- 2× level shifting for DAC NMOS switches
- -200mV charge pump level shifter for DAC PMOS switches

0.3V $\Delta\Sigma$ Circuit Design

Sampling switch

To increase $g_{ds,ON} // I_{OFF}$

- *Cascading*
- Feedback amplifier
- 3× clock boosting for gate of NMOS switch
- -200mV charge pump level shifter for gate of PMOS switch



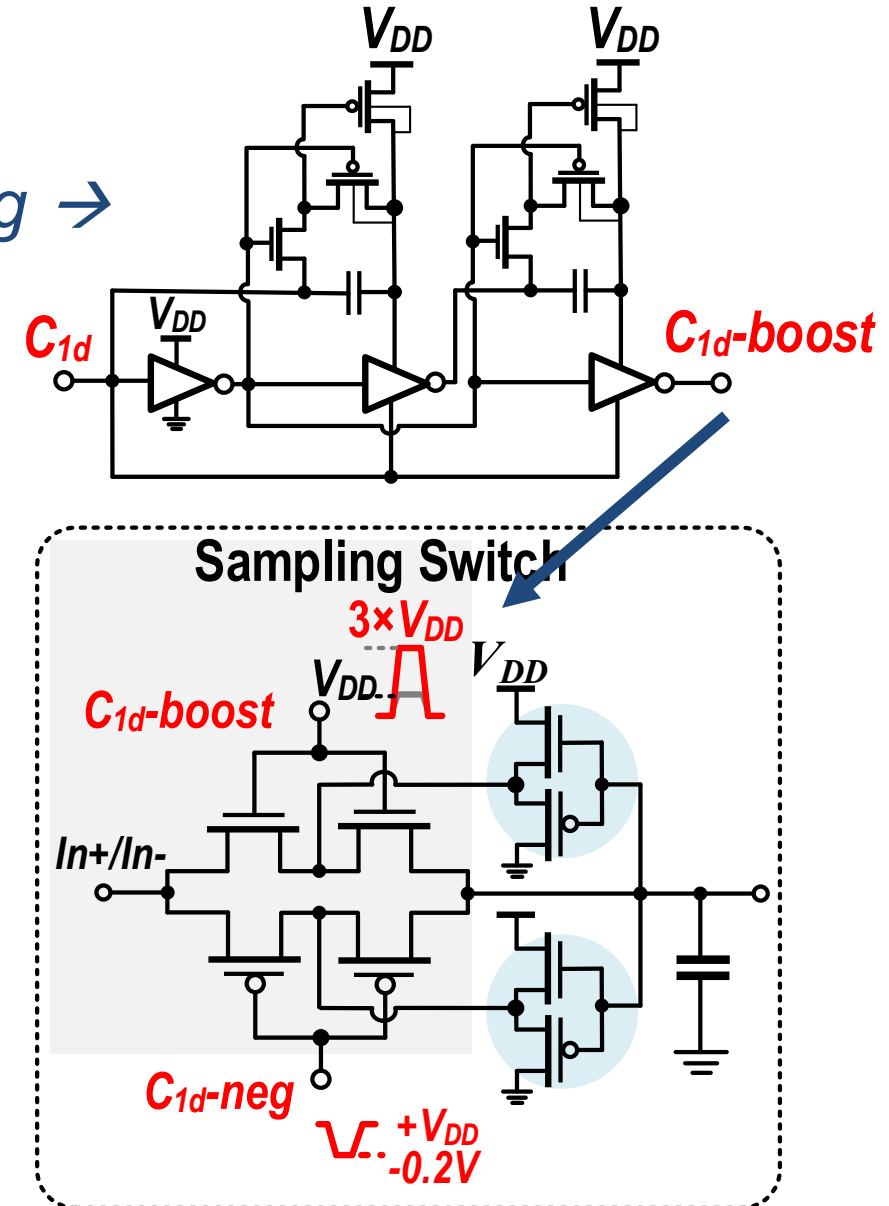
0.3V $\Delta\Sigma$ Circuit Design

Sampling switch

To increase $g_{ds,ON} // I_{OFF}$

- Cascading
- Feedback amplifier:
- **$3\times$ clock boosting for gate of NMOS switch**
- -200mV charge pump level shifter for gate of PMOS switch

$3\times$ Clock Boosting \rightarrow

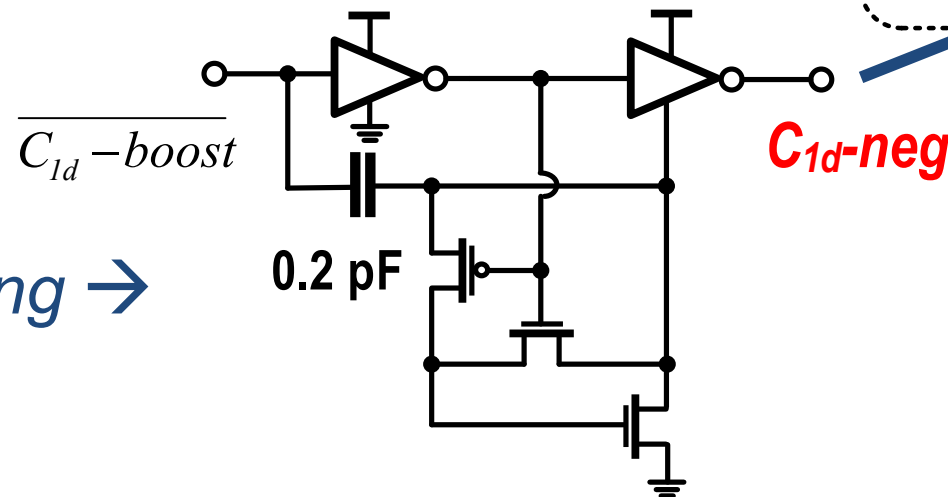
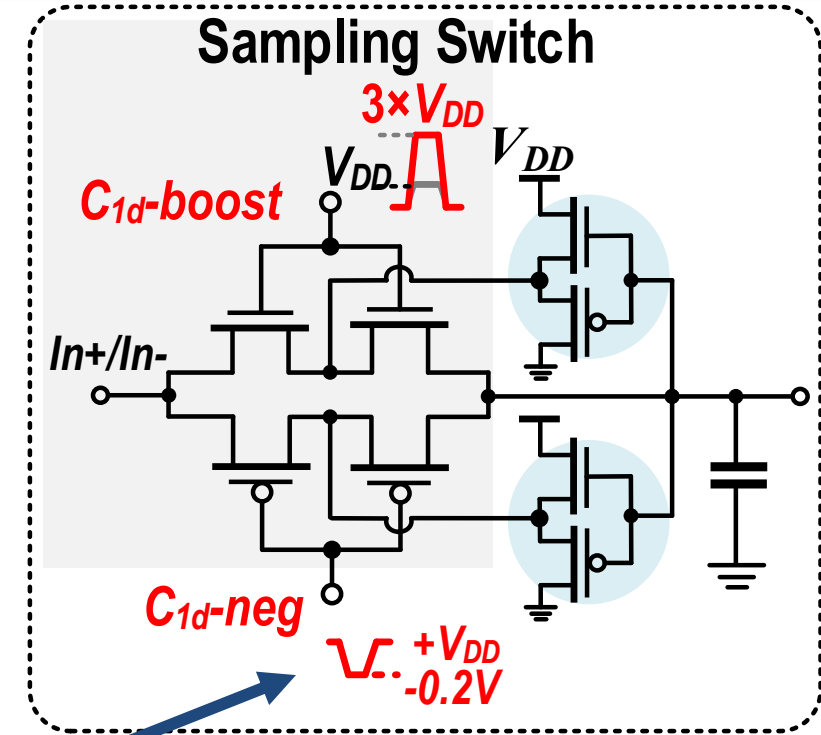


0.3V $\Delta\Sigma$ Circuit Design

Sampling switch

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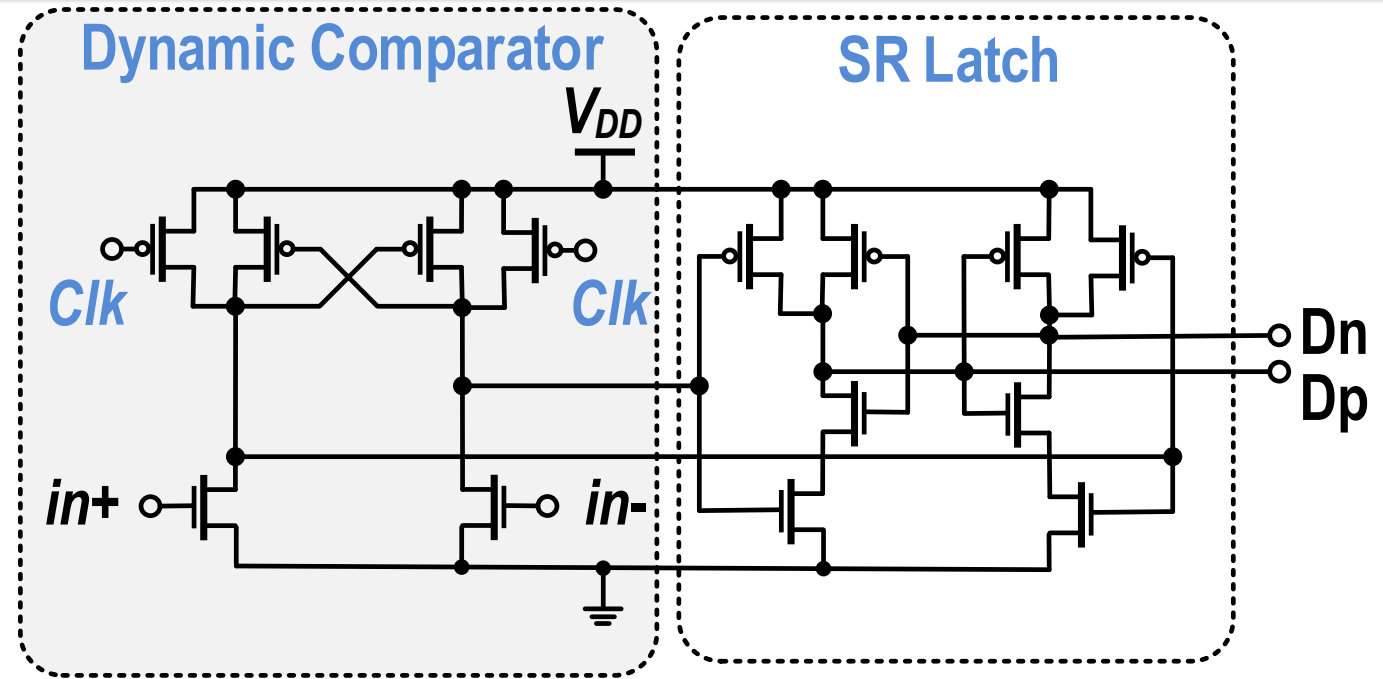
Negative Level Shifting →

→ Increases SNDR by 3dB

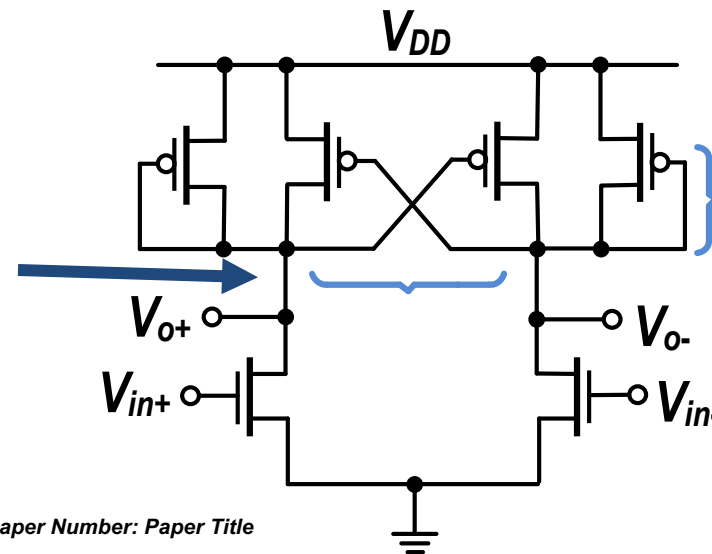
0.3V $\Delta\Sigma$ Circuit Design

0.3V Single-Bit Quantizer:

- **Dynamic comparator**
- **Preamplifier**
 - Low- V_{th} transistors
 - Stacking only two transistors
 - Positive feedback gain-boosting



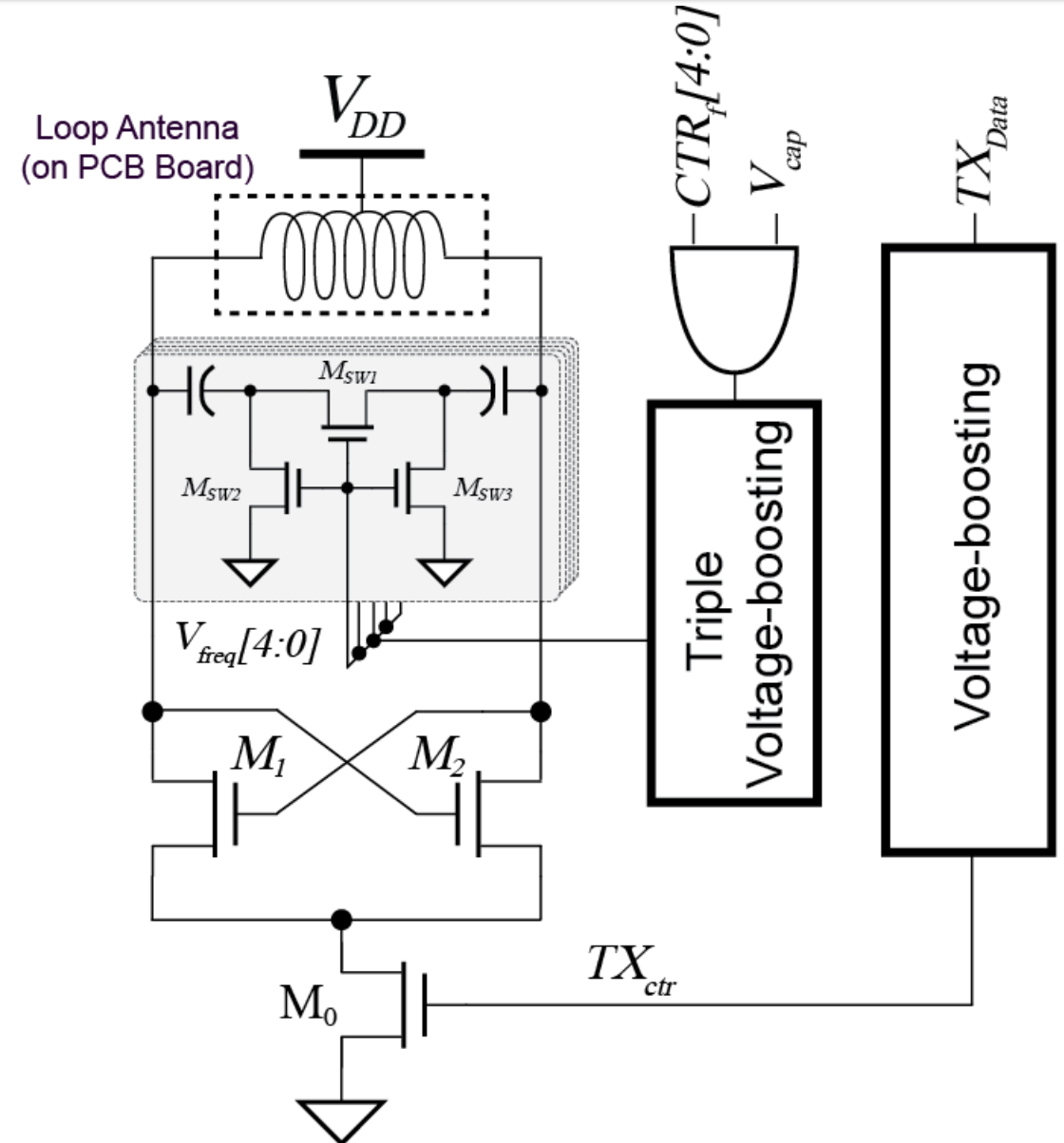
*Negative
Conductance
Gain-Boosting*



*Offering inherent
Common-Mode
Feedback*

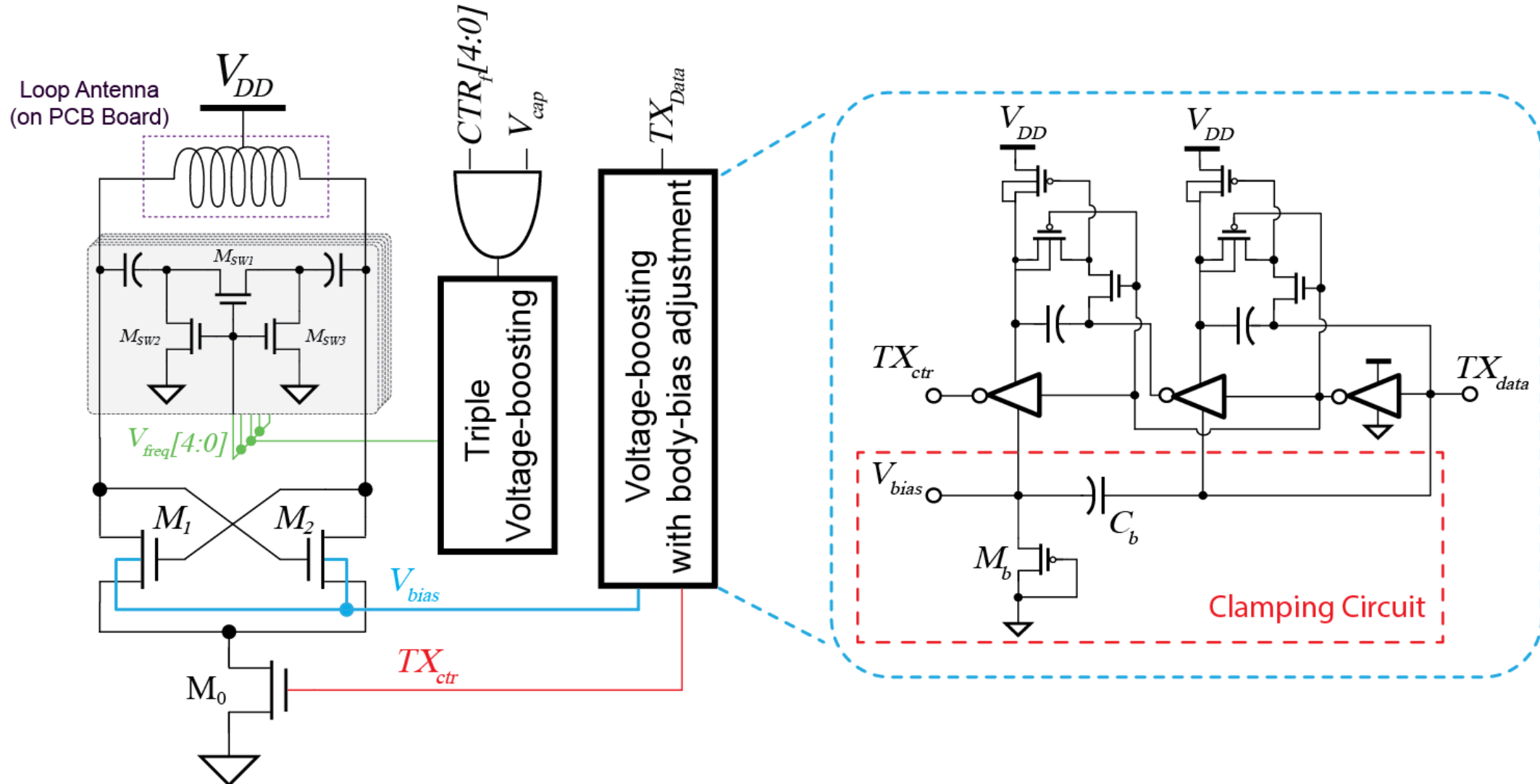
TX Design

- **Direct-RF power oscillator (RFPO)**
 - Inherent impedance matching to antenna
 - Low leakage power during inactive phase
 - OOK-modulation
- **0.3-0.4V low supply voltage**
 - Limits the efficiency, I_{ON}/I_{OFF} ratio and start-up time
 - Boost the power supply
 - Large inductors or capacitors



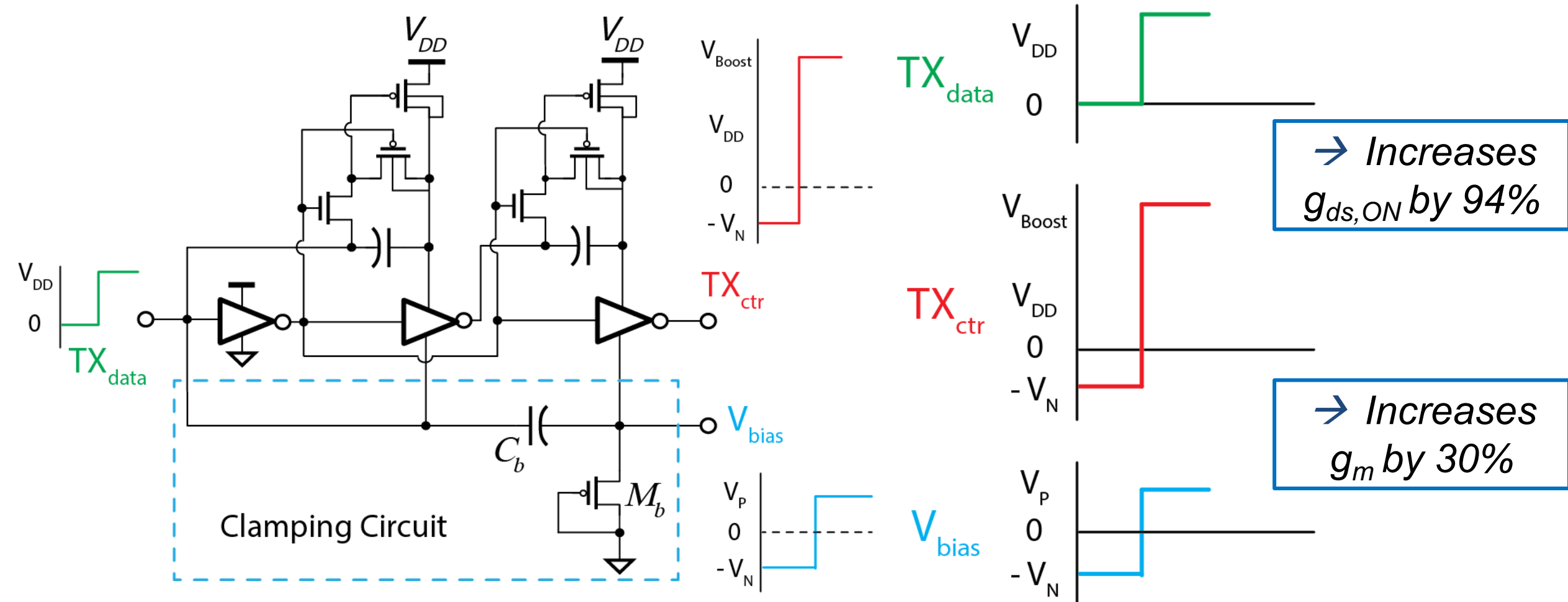
TX Design

- TX control circuit for improving I_{ON}/I_{OFF} ratio of transistors and start-up time



TX Design

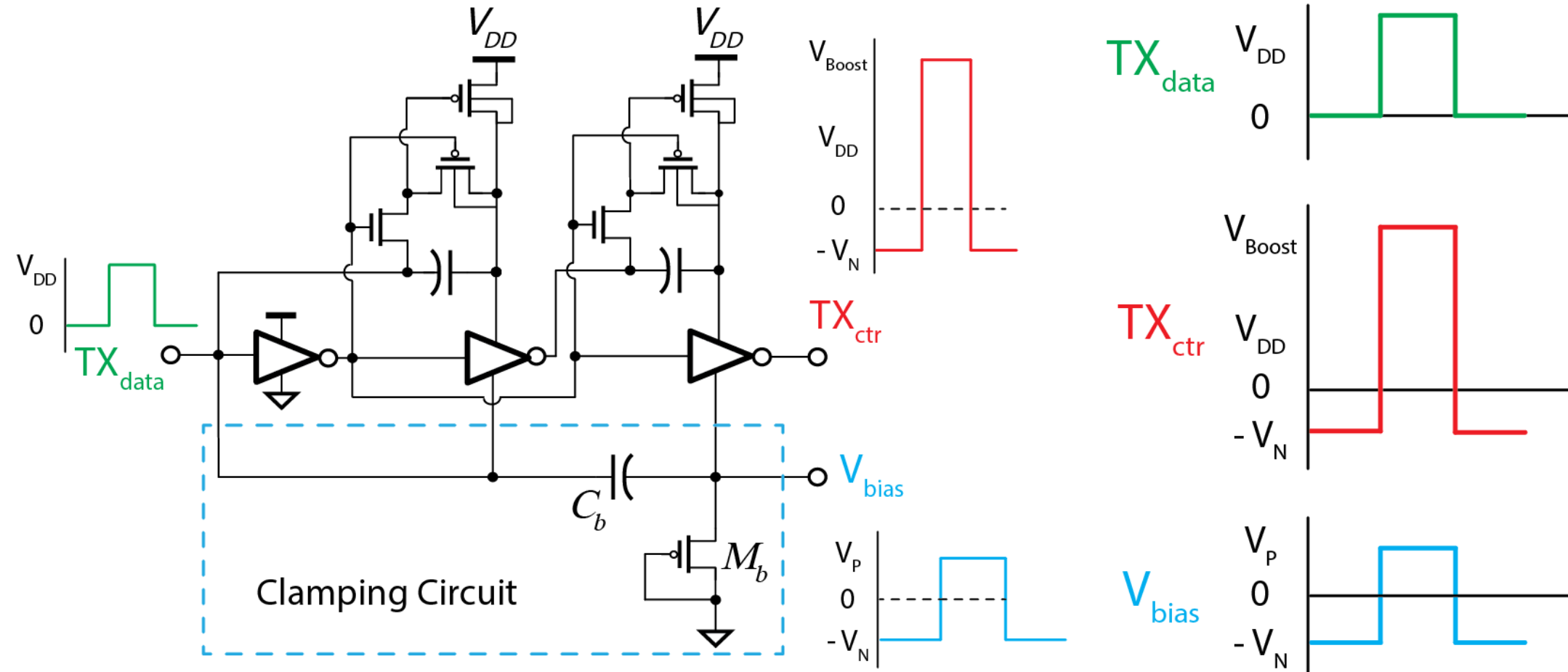
- When $TX_{data} = '1'$, TX_{ctr} is boosted $3\times$ and V_{bias} is set to $\sim V_{th}$



\rightarrow Improves start-up time and power-efficiency

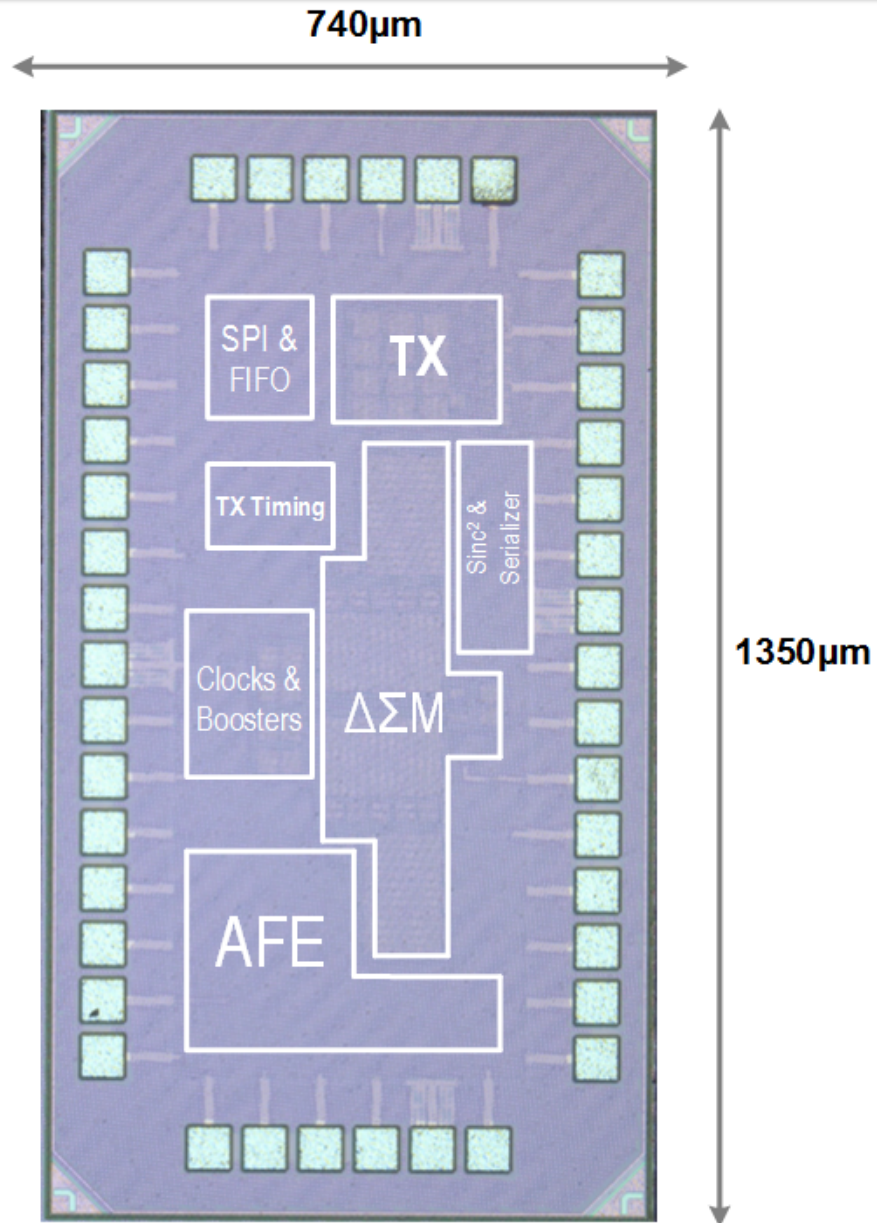
TX Design

- When $TX_{data} = 0$, the V_{bias} is set to $\sim -V_{th}$



→ Helps reduce off-leakage up-to 92% during TX inactive phase

Die Micrograph



TSMC 65nm LP CMOS
1 mm² with pads

On-chip $\Delta\Sigma$ ADC clocks

Power supply: 0.3-0.4V

Power break-down @ 0.3V:

TX active power: 30.1µW

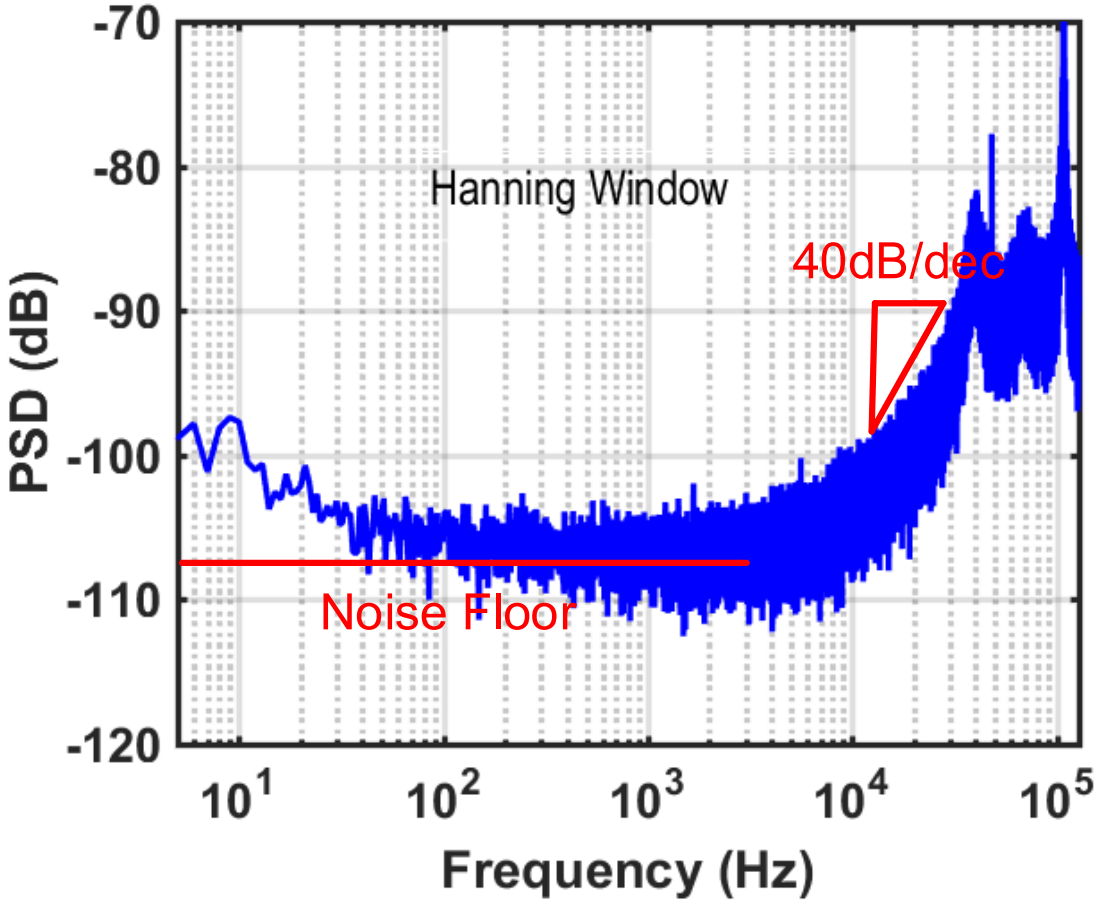
TX standby power: 2.88nW

$\Delta\Sigma$ ADC active power: 180nW

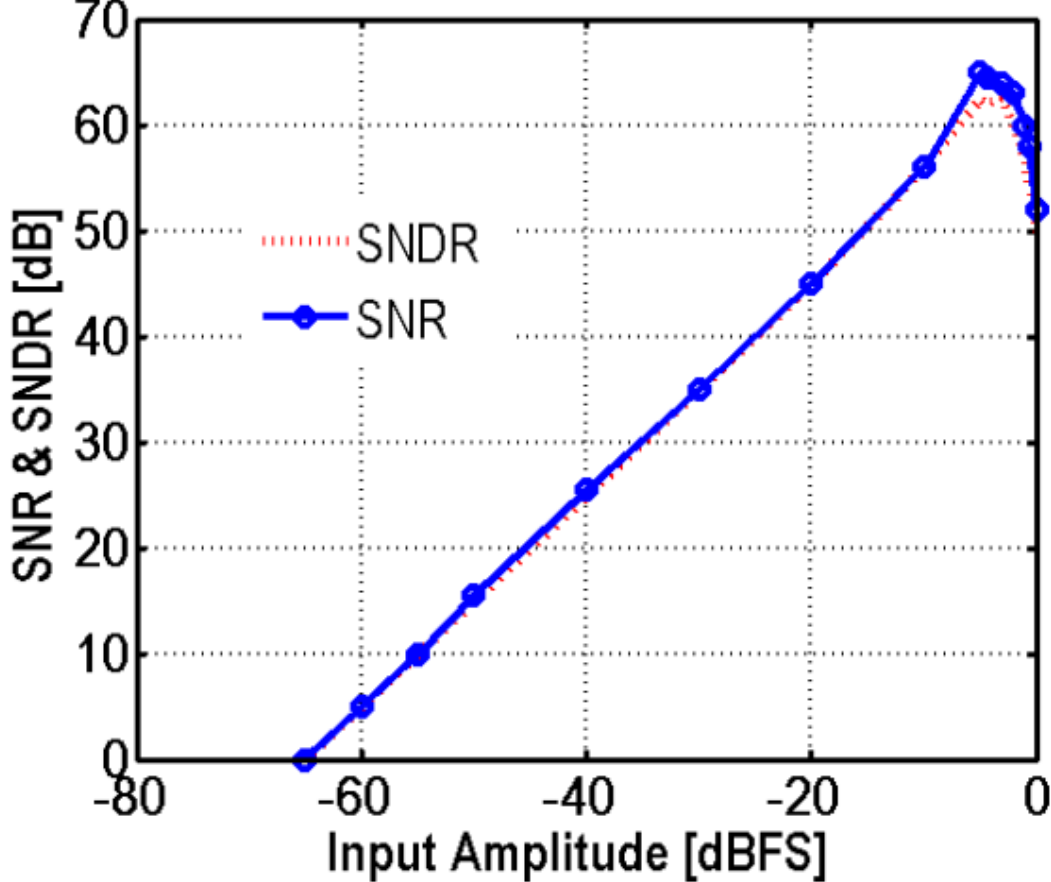
$\Delta\Sigma$ ADC standby power 2nW

In-Vitro Experimental Results

PSD of $\Delta\Sigma$ Modulator

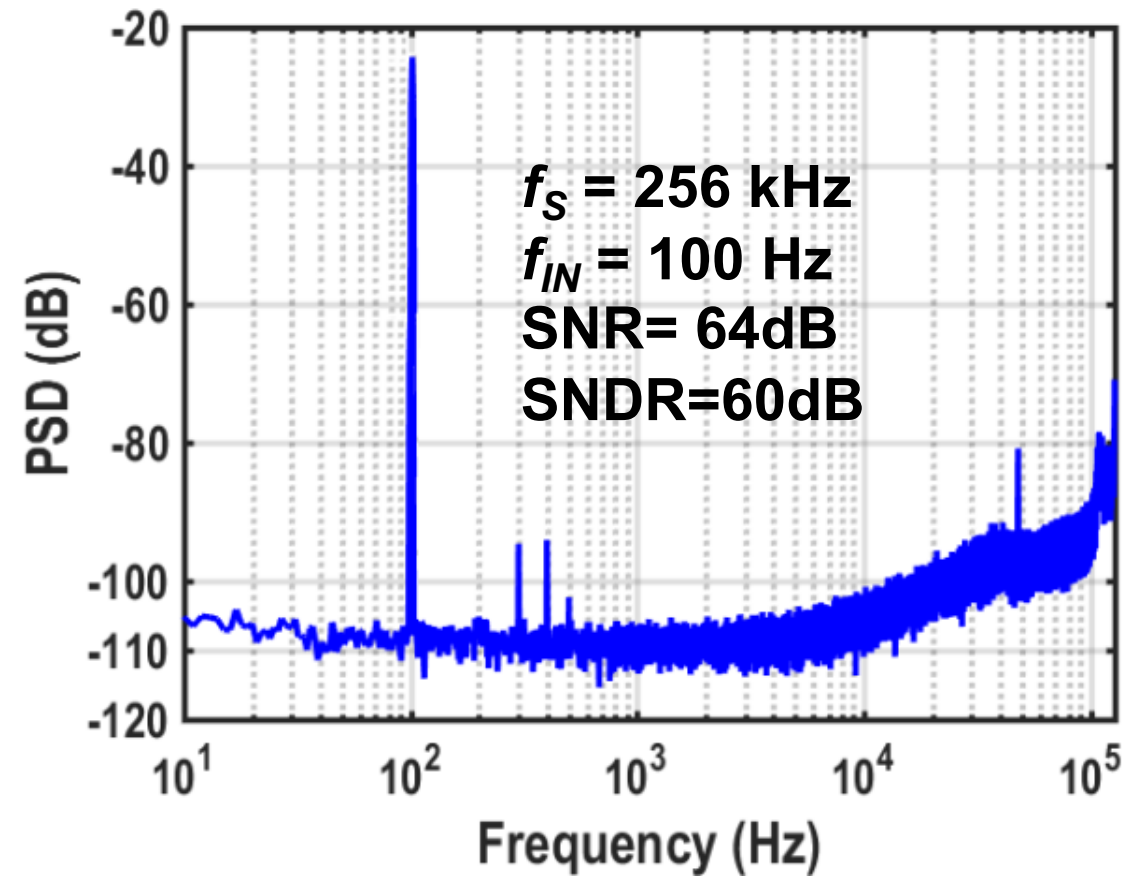


2nd-order noise-shaping
Noise floor: -105dB



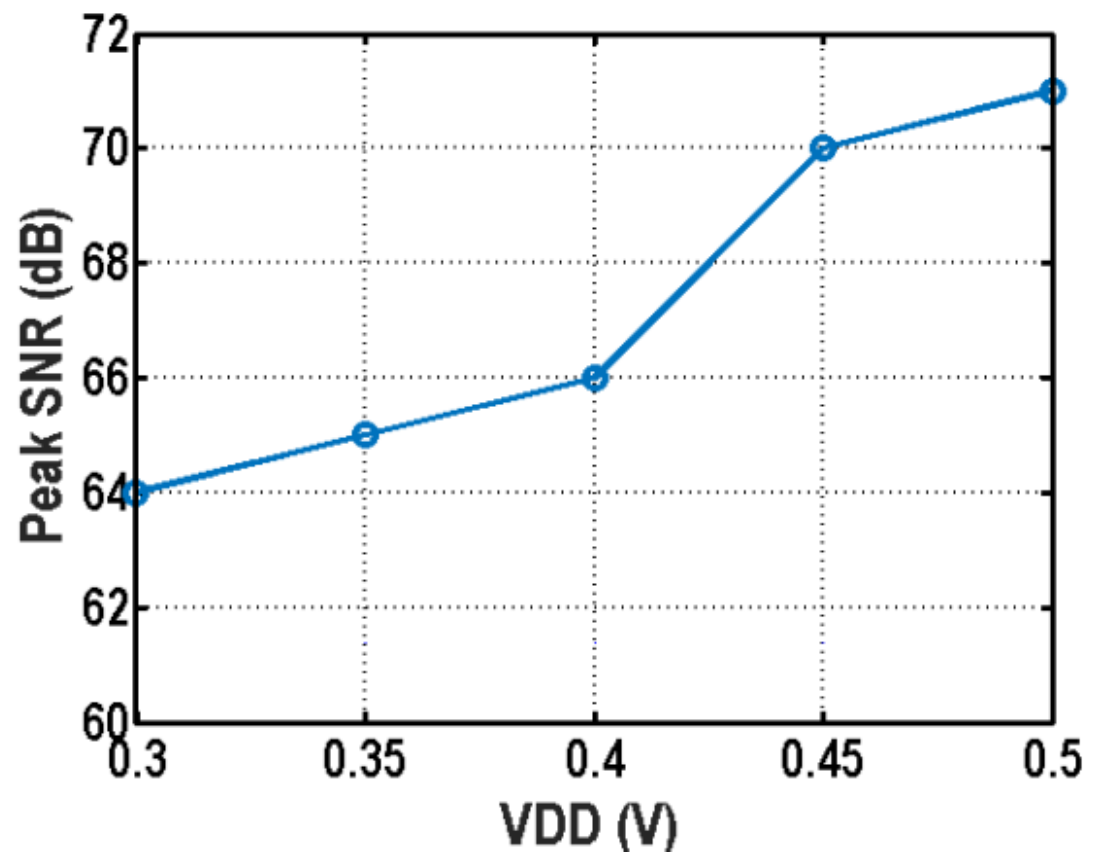
SNR = 64dB / SNDR = 60dB

PSD of $\Delta\Sigma$ Modulator



$V_{DD} = 0.3\text{V}$

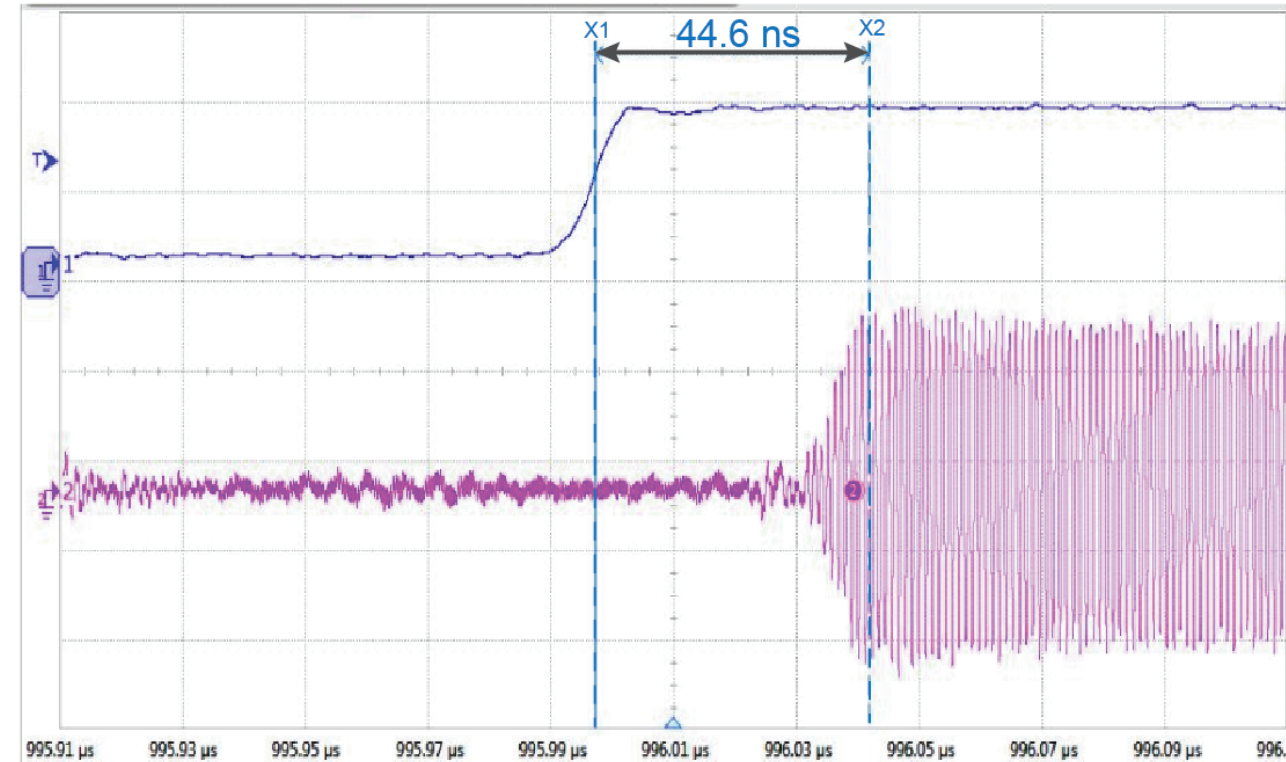
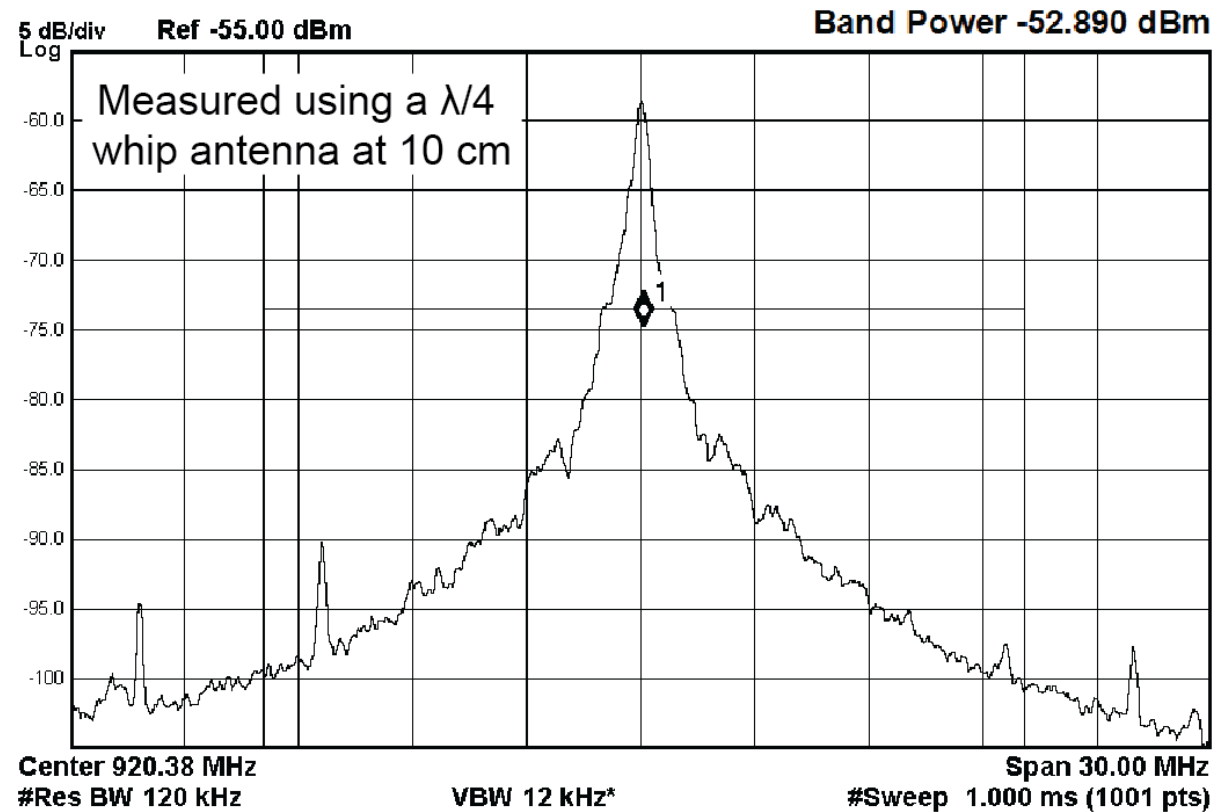
- Sampled at 256kHz clock



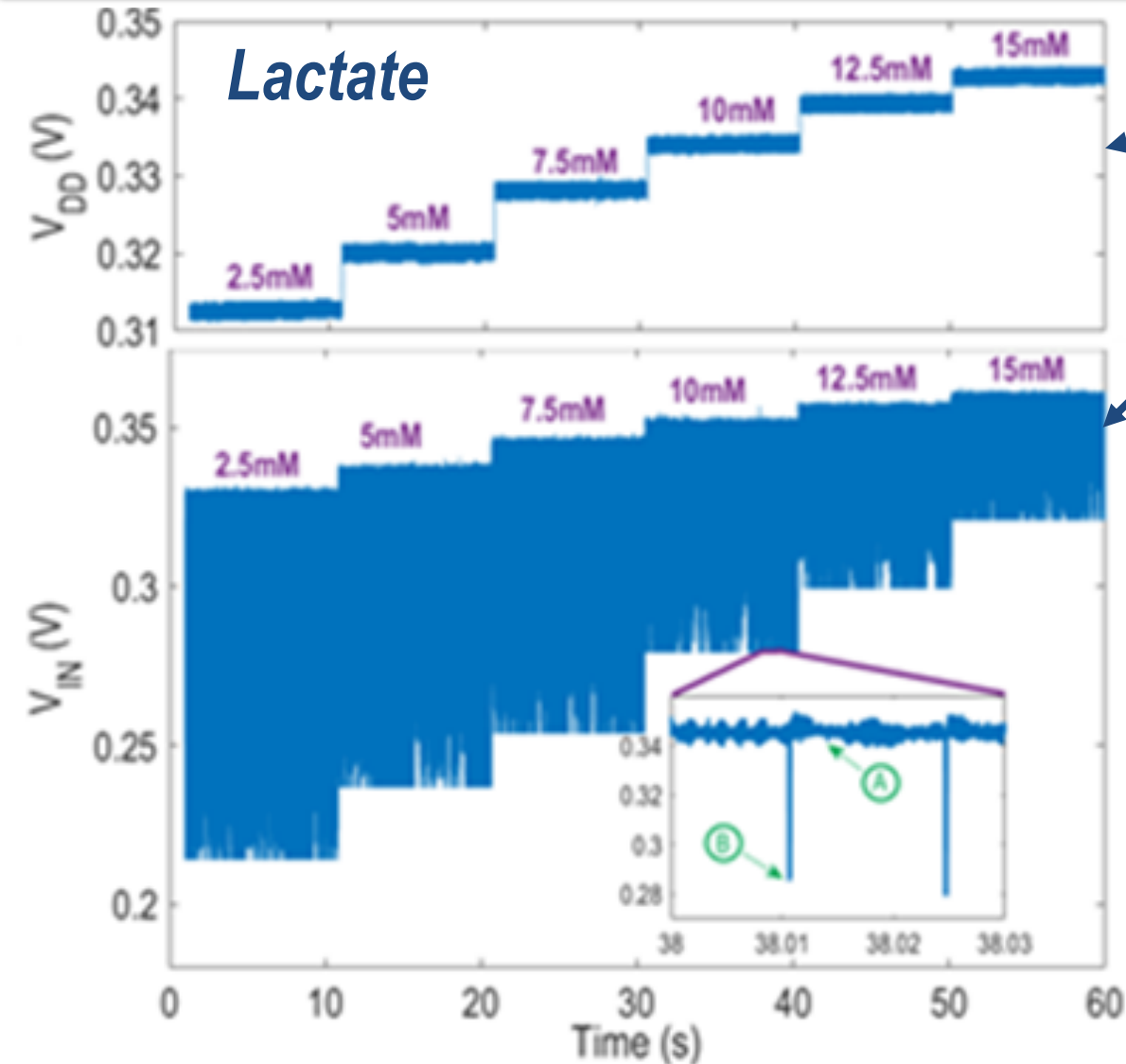
- ADC is robust to supply variation
SNR = 71dB @ 0.5V
SNDR = 65.5dB @ 0.5V

TX Performance

- Operating at 1Mbps, the TX output power $> -53\text{dBm}$ at 10cm with $V_{DD}=0.3\text{V}$
- Consumes 30pJ/bit at 0.3V
- Start-up time $< 44.6\text{ns}$

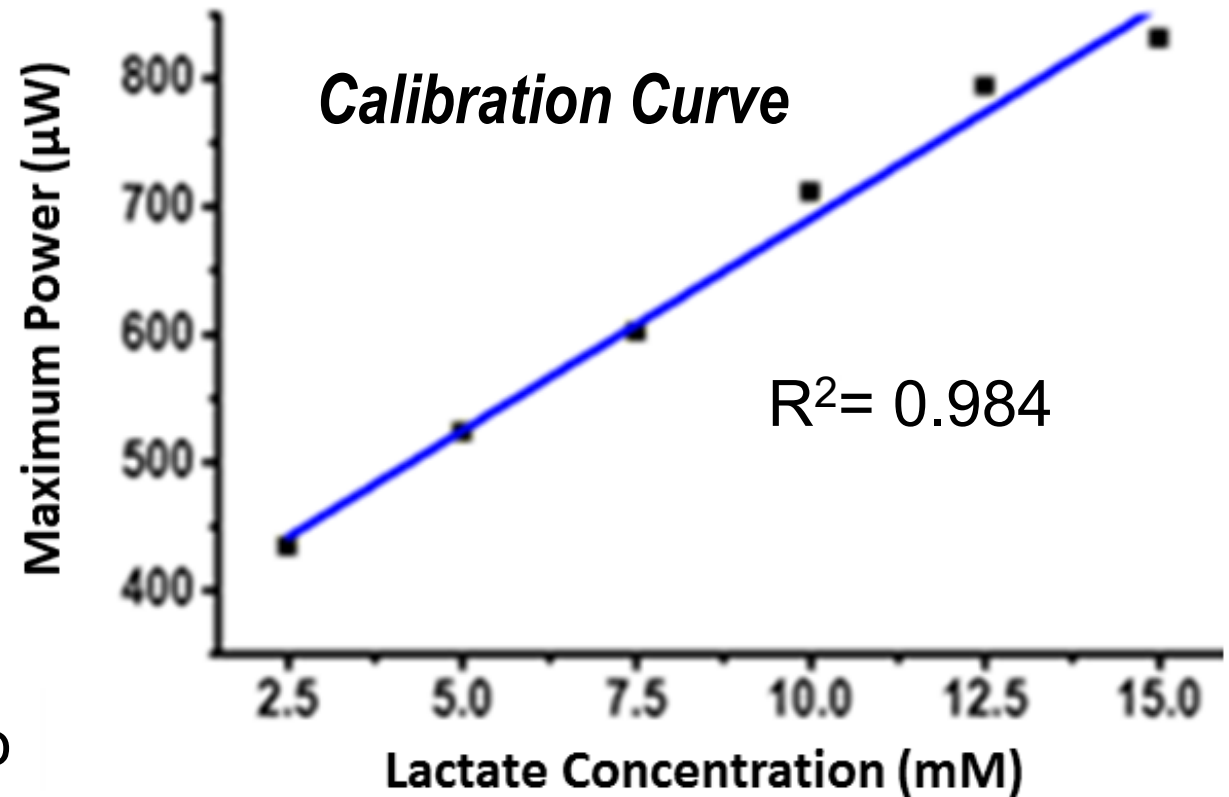


In-Vitro Experiments (Lactate)



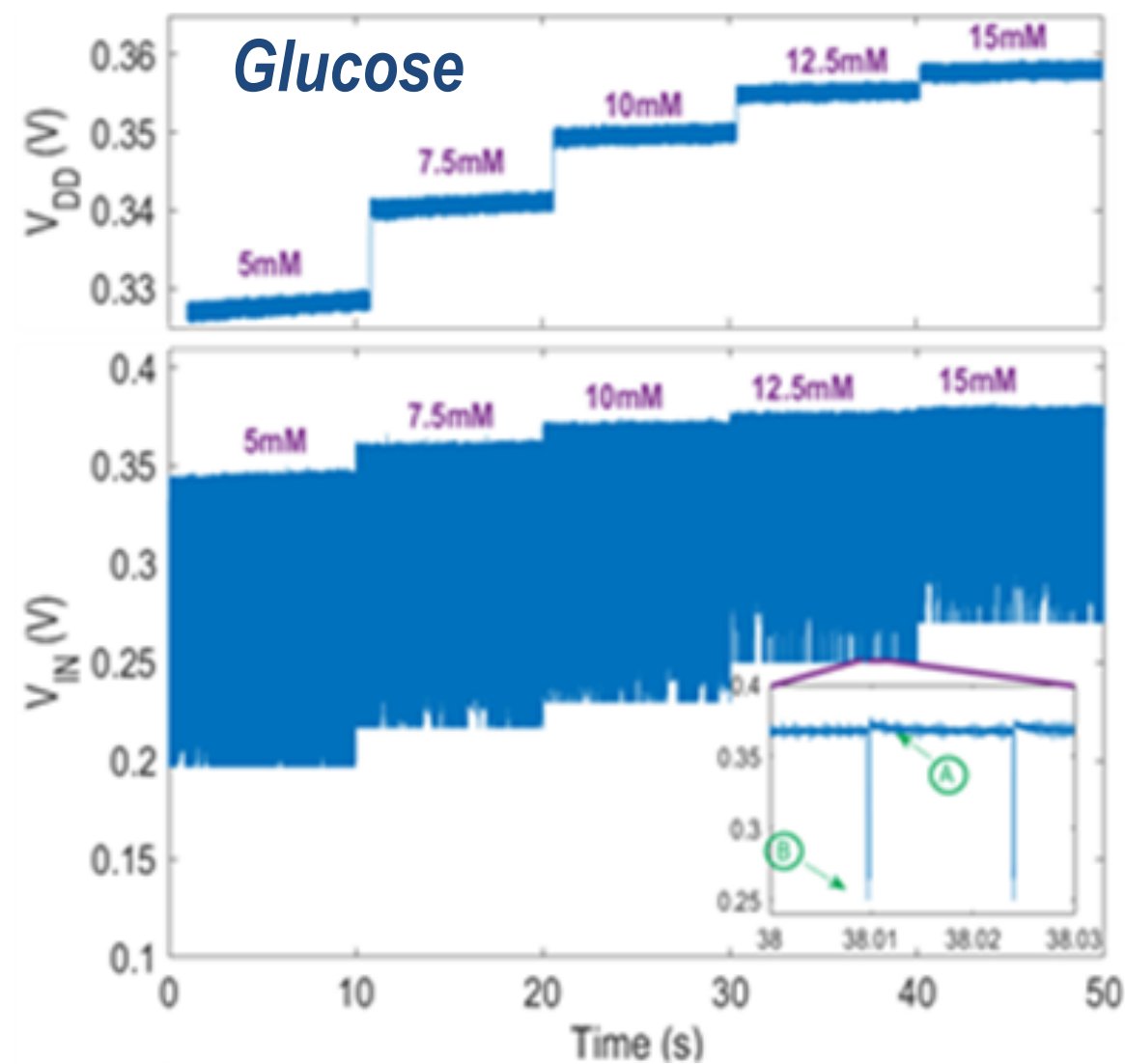
Dynamic V_{DD} variation

BFC output power



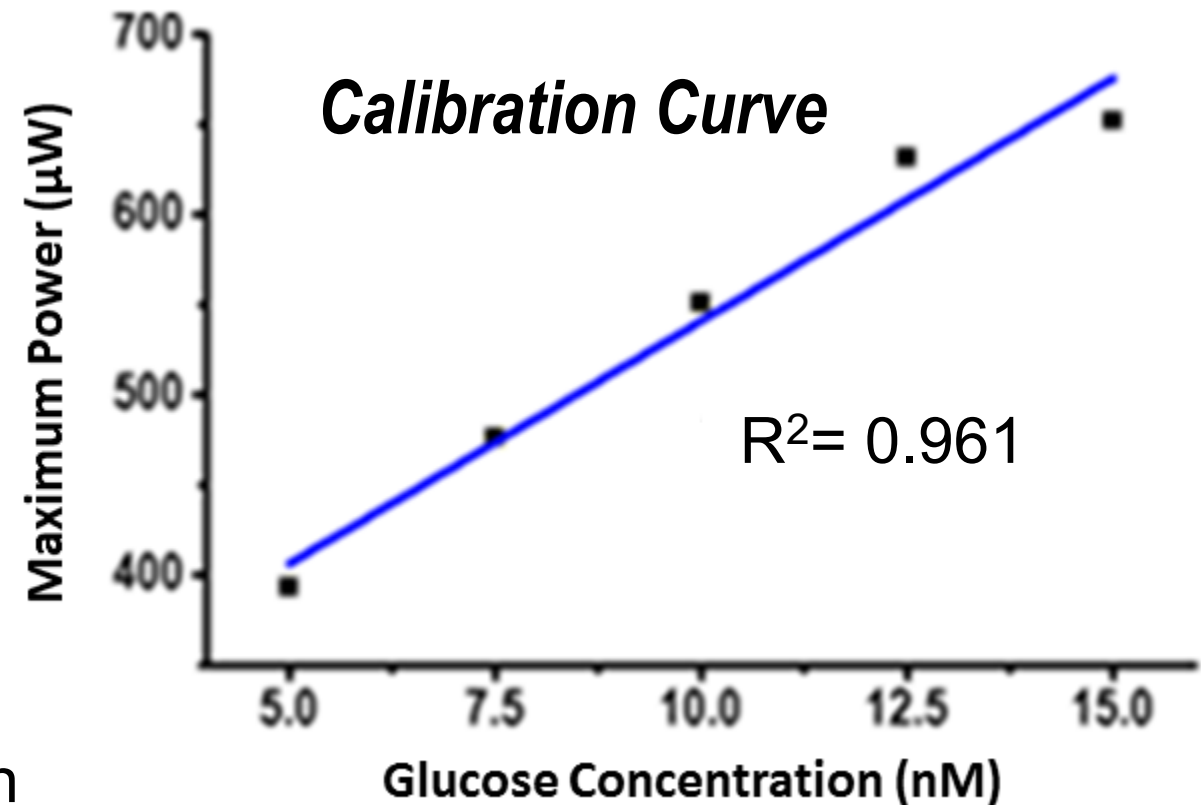
- Physiologic ranges in human perspiration

In-Vitro Experiments (Glucose)



Dynamic V_{DD} variation

BFC output power



- Physiologic ranges in human perspiration

Conclusions

- **Demonstration of an integrated self-powered biochemical sensing system with digital wireless readout**
- **At 1% duty-cycle, the ADC and TX consume an average of 1.15 μ W**
- **Passive $\Delta\Sigma$ ADC and RF power oscillator circuits enabled 0.3V Biosensor**
- **In-Vitro glucose/lactate measurements represent physiologic ranges of human perspiration**

Conclusions

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- **At 1% duty-cycle, the ADC and TX consume an average of 1.15 μ W**
- **Passive $\Delta\Sigma$ ADC and RF power oscillator circuits enabled 0.3V Biosensor**
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Thank you for listening!